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THESIS

AN ANALYSIS OF A PUFF DISPERSION
MODEL FOR A COASTAL REGION

by

Stephen K. Rinard

June 1982

Thesis Advisor:

G. E. Schacher

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An Analysis of a Puff Dispersion Model for a Coastal Region

by

Stephen K. Rinard
National Weather Service
B.S., Texas A&M University, 1964

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requirements for the degree of

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ABSTRACT

The Risø National Laboratory, Roskilde, Denmark, atmospheric puff dispersion model has been tested for an atmospheric-marine environment. This three-dimensional model simulates the release of Gaussian pollutant puffs and predicts their concentration as they are diffused and advected downwind by a horizontally homogeneous, time-dependent wind. Atmospheric characteristics such as turbulence intensity, potential temperature gradient, buoyant heat flux and maximum mixing depth have been considered. Model predicted pollutant concentrations have been compared to airborne sampled observations. The effect of coastal turbulence not observed by the single point meteorological measurements made onboard ship greatly affects the advection and diffusion of a plume as it moves onshore. Additional measurements/predictions particular to the coastal area will have to be incorporated into the model for it to accurately predict the onshore movement of pollutants.

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I. INTRODUCTION

The downwind transport and distribution of atmospheric pollutants from an isolated source over land or water has become an important environmental factor in today's society. The need to understand the distribution of smoke, unpleasant or potentially harmful foreign gases and perhaps radioactive debris from a nuclear powerplant accident are becoming more and more essential for industrial operations and construction planning. The dispersion of such atmospheric pollutants is commonly modeled by a standard Guassian plume model which computes one-hour average plume characteristics.

The Meteorology Section of the Risø National Laboratory, Roskilde, Denmark, has recently developed a puff model for prediction and simulation of atmospheric pollutant diffusion. The model considers individual puffs of pollutants with specific release rates that are advected by a horizontally homogeneous wind over a grid. The wind input may be either the measured wind from a single point, a spatial average or a wind simulation. The model simulates the instantaneous plume characteristics by adding a group of puffs, growing in size, as they advect with the wind. A Guassian plume model, on the other hand, provides a time

averaged concentration pattern based on a single time average wind vector. In the puff model, the plume advects with a time series of actual wind data. Thus, the puff model is able to predict time varying concentration distributions in actual changing wind conditions, making it an appropriate tool for dynamical computations of downwind dispersions of pollutants.

A basic comparison of a puff model simulation and a typical plume is illustrated in Fig. 1. Looking from above, the instantaneous behavior of a plume being advected from a source by the wind is shown. The outer cone-shaped contours represent the outer limit of the plume boundary and are identical in both Figs. 1 (A) and (B).

Fig. 1(A) shows an instantaneous depiction of an actual plume. The long-term average plume concentration is shown on the extreme right as a smooth curve with a maximum on the central axis. Also shown is the instantaneous plume concentration considered realistic but is of such a short time scale that it cannot be predicted or easily measured.

The puff model prediction is depicted in Fig. 1(B). The circles show the boundaries of individual puffs of pollutants released from the source. These puffs are advected

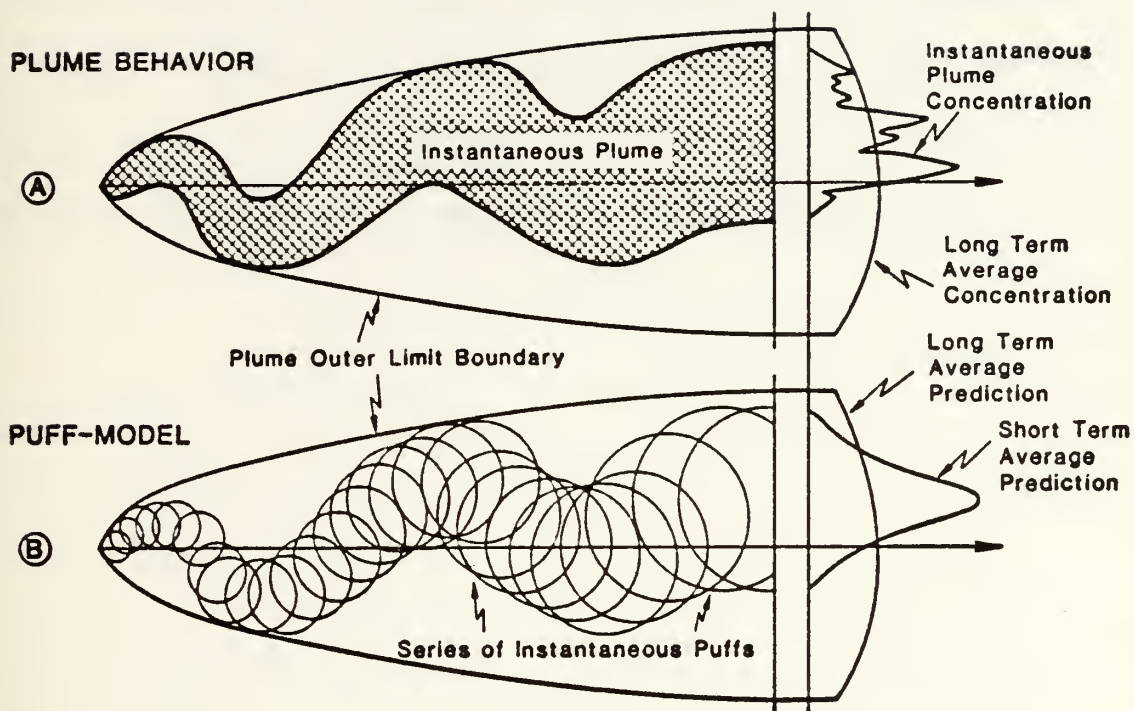


Figure 1. Instantaneous Behavior of a Typical Plume and a Series of Puffs from a Puff Model

and diffused downwind by a frequently updated wind. The long term average concentration prediction of the puff model is expected to be identical to the long term concentration of Fig. 1 (A). The short term average pollutant prediction, a Gaussian curve shown on the extreme right, is not completely realistic but is a reasonable approximation to the instantaneous plume concentration profile.

The purpose of this thesis is to evaluate and test the general characteristics and capabilities of the Risø puff model. The adjustable input data will be varied and predicted results for various input combinations compared. A preliminary comparison will also be made between predicted results and data collected from a coastal region using observed meteorological forcing data as model input.

II. RISØ PUFF MODEL

A. GENERAL CHARACTERISTICS

The Risø Puff Model is a three-dimensional computer model used for the prediction and/or simulation of the diffusion and advection of atmospheric pollutants. The puff model technique is to simulate a plume with Gaussian shaped puffs with specified release rates within a specified grid. The initial size of the puffs is normally one meter in diameter although this can be easily adjusted. The amount of material in a puff is the release rate times the elapsed time between puffs. Therefore, a long elapsed time between puff releases results in a higher initial puff pollutant concentration than a short time interval. This should not normally be of concern if an adequate balance is maintained between grid size, advection speed and puff release rate.

The location of the puffs on the grid is determined by computing their movement for a finite time step using a measured wind field. The growth and buoyancy of the puffs are computed from simultaneous specifications of atmospheric turbulence intensity and stability and from buoyant heat

flux at the source. An inversion cap through which pollutants cannot pass and the source height where pollutants are released are variable and can easily be adjusted. Grid distances within the model may vary from meters to kilometers and time durations from seconds to hours are possible.

This puff model has the capability of monitoring a maximum of twenty-five sources of puffs and its grid may contain up to 100 puffs. A puff source can be located anywhere on the grid and have a unique release rate, start and stop of release time, and heat production. When the center of a puff moves outside the boundaries of the grid (either horizontally or vertically), that particular puff is dropped from memory. In this way the model does not store irrelevant puff information, thus keeping computer memory requirements to a minimum.

A variable to control the amount of reflection/absorption of the pollutant by the surface is easily adjusted in the puff model. Such a parameter is of great value both in actual dispersion problems and also for gaining understandings of the plume/surface relationship.

The model calculates the concentration at each grid point by summing the contributions from surrounding puffs

for each advection step. The grid concentrations can be allowed to accumulate or simply be updated with the latest instantaneous value. A minimum grid concentration of interest can be set to reduce computer run time by dropping concentrations too small to be of interest.

The output of the model contains periodic results of puff locations and concentrations as well as initial input verification. The time interval for the periodic results is adjusted by the input data. This recurrent lineprinter output contains:

- X-Y plane plots showing the position of the sources and of puffs inside the grid,
- X-Z plane plots of puff positions for evaluating plume rise for each vertical level of interest, and
- a table listing of the grid point concentrations for each level.

A computer drawn contour chart of the magnitudes of the pollutant concentrations is also available.

When considering distance between gridpoints ($\Delta x, \Delta y, \Delta z$), only spatial resolution and computer resources need be considered. Calculated concentration accuracy is not related to the grid-point separation. To insure that no essential information on individual puffs is "hidden" between grid points, the grid separation should be adjusted dependent upon the size of the puffs at the downwind distance of interest. Other specific model configuration considerations are described in the following sections. They are also discussed in more detail in the model behavior chapter.

B. WIND FIELD

Once a puff is released, it is advected based upon wind data measurements at a single point only, normally the release point. This limits the validity of the model to situations where the wind field and turbulence can be assumed to be horizontally homogeneous throughout the grid. It is therefore important to insure that the data obtained from such a single point measurement is representative of the wind structure for the whole area of interest.

The wind data are normally obtained in the form of a horizontal velocity time series. A vector sequence is formed

by averaging over a convenient interval. These data are read into the model after being segregated into turbulence classes as discussed in the next section.

C. TURBULENCE INTENSITY AND DIFFUSION

The growth/diffusion of a puff depends upon the turbulence intensity. To account for this growth, the puff model applies the theory for relative diffusion suggested by Smith and Hay (1961).

The turbulence intensity is defined to be the standard deviation (σ) of the wind direction (in radians) squared. The σ values are collected for the same short time periods as the wind speed measurements used to advect the puffs. Therefore, the intensity of the turbulence which governs the relative diffusion of the puffs, can be adjusted along with the the advecting wind speed after each time step, if conditions warrent.

A very low value of turbulence intensity (as 0.0002) represents a small standard deviation (0.9), normally a stable atmosphere and a weak puff dispersion/diffusion. As the atmosphere becomes more unstable, the turbulence intensity increases along with an increase of σ values and plume dispersion/diffusion. While these characteristics are

representative of turbulence over land, they can be applied to over water cases in a broad sense.

D. PLUME RISE

In the vertical direction, puff-rise can be accounted for by Briggs (1970) plume rise theory. In this case buoyancy is assumed to be conserved (adiabatic motion), and pressure forces, molecular viscosity and local density changes are considered small and are neglected. The rate at which a puff rises as it is advected downwind is a function of the buoyancy flux, wind speed, puff distance traveled and stability of the atmosphere. Plume rise is considered separately for each individual puff.

E. REFLECTION

The interaction of the pollutant with the surface is adjustable and can be easily changed in the input data. Total reflection or absorption or a fraction between the two can be used.

F. LIMIT OF MIXING DEPTH

The effect of an atmospheric lid (inversion) can be applied in the model to limit the vertical movement of the pollutant. The model does not permit the plume to rise

above this cap. When a maximum mixing level is in effect, it acts to totally reflect the pollutants in the same manner as total reflection at the surface. This mixing cap would act as an inversion when the puff would be expected to grow much more readily in the horizontal than in the vertical direction.

III. DATA COLLECTION

An intensive field tracer study was performed during the fall of 1980 and winter of 1981 in the Santa Barbara Channel area of the California coast. The work was supported by the Bureau of Land Management (BLM) and performed by the Environmental Physics Group of the Naval Postgraduate School (NPS) and AeroVironment Inc (AV), Los Angeles, CA. This study was designed to help validate and/or modify Gaussian dispersion models for coastal use and to build a data base for future model development. Air pollution models in current use have not been adequately validated for the over-water regime.

In the experiment, a tracer gas (SF_6) was released several miles offshore from the NPS Research Vessel (R/V) Acania. Ambient gas concentrations as low as 10 parts per trillion (PPT) were determined by an array of land based sensors, from a small boat and at various levels by an aircraft equipped with a continuous SF_6 analyser. A chart of the experimental area and locations of the various platforms is shown in Fig. 2.

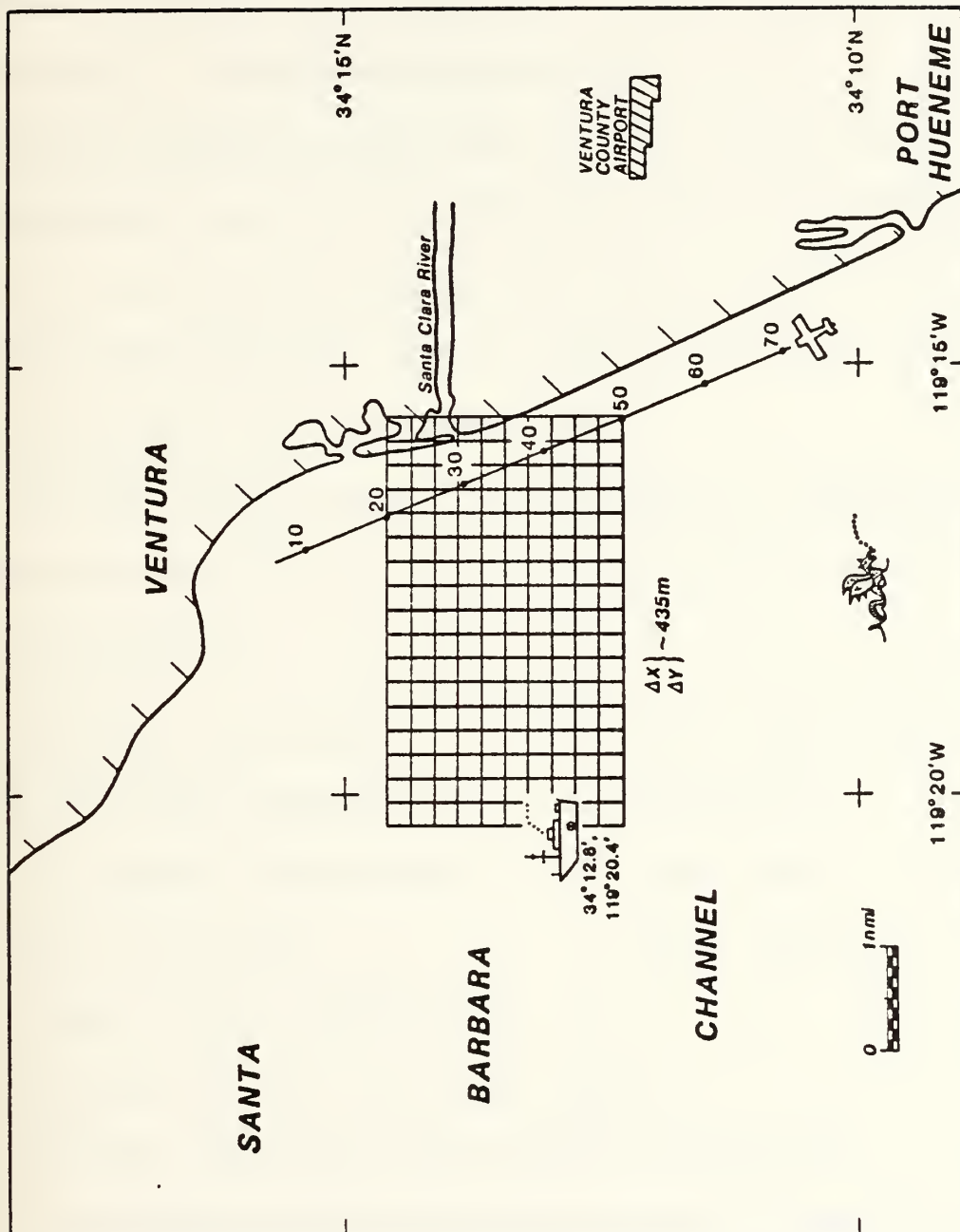


Figure 2. Experimental Area showing Locations of R/V Acanla, Aircraft track and Numerical Grid.

The aircraft flew through the plume at various elevations offshore and overland. The plume transect tracks pertinent to this study were made parallel to the coast approximately one-half mile offshore. The airborne sampling consisted of instantaneous concentrations (PPT) at selected points at different levels over a period of six hours. The observations, recorded at locations 10-70 at altitudes of 61 and 91 m above MSL on January 29, 1980 are shown in Fig. 3. Average concentrations over the noted time period are shown at the bottom of each altitude block.

The following marine meteorological parameters were measured onboard the R/V Acania while anchored approximately 7.4 km offshore:

- | | |
|---|------------------|
| •relative wind speed | •air temperature |
| •wind speed fluctuation | •dew point |
| •sea surface temperature | •ship roll |
| •sky cloud cover | •ship location |
| •relative wind direction | |
| •inversion height (acoustic sounder) | |
| •vertical temperature and humidity profiles | |

(shipboard radiosonde launch every 12 hours).

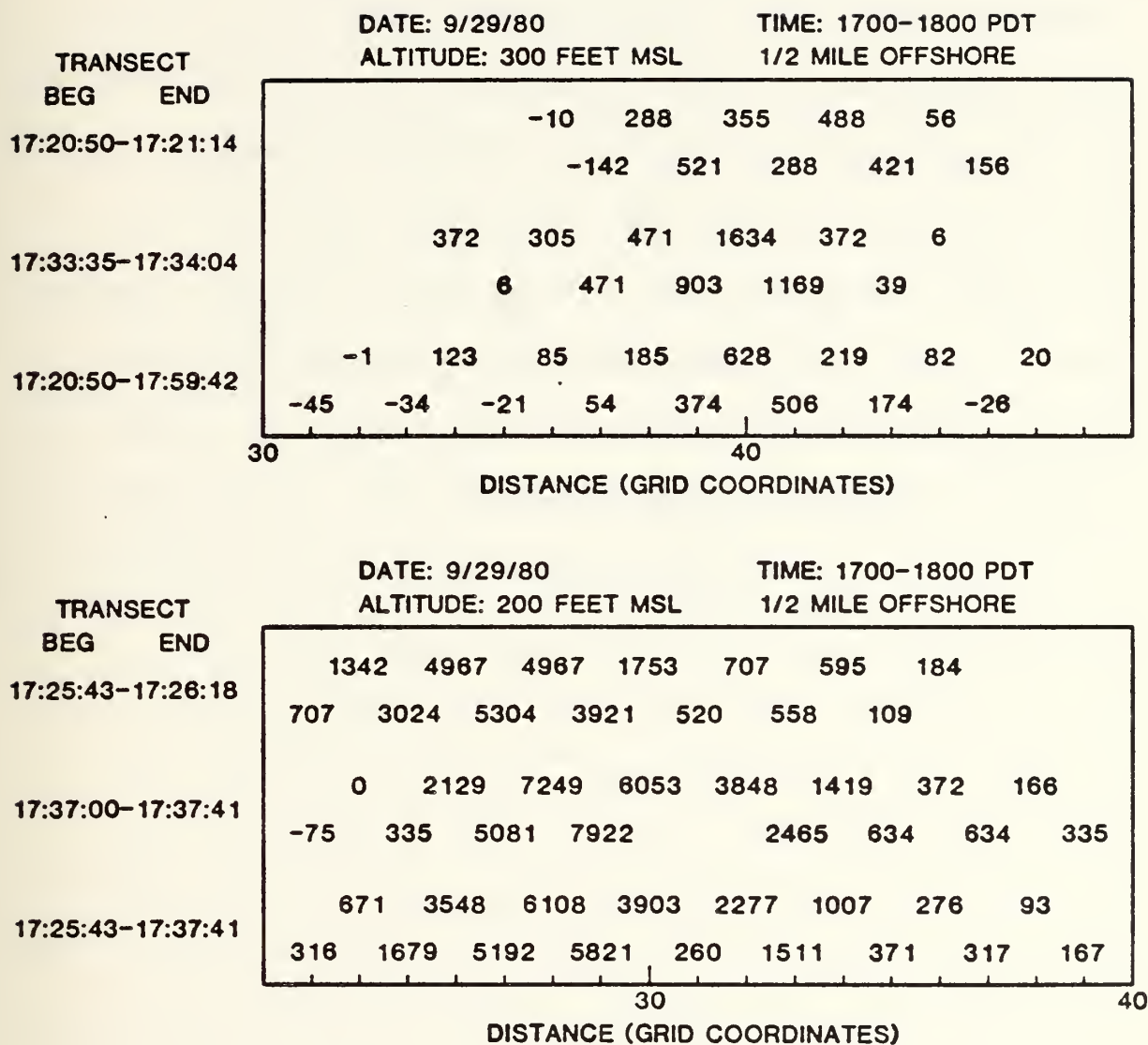


Figure 3. Aircraft observed Plume Concentrations (PPT) at Grid Coordinates at 61 and 91 m above MSL, 29 September 1980.

The tracer gas was released at a fixed rate through the exhaust of one of the ships motor generator sets. The generator was run at a constant speed resulting in a constant stack temperature and flow rate.

The above collected meteorological information enabled the data grid to be established and the atmospheric wind field, turbulence intensity, stability and buoyancy flux to be derived for inputs into the puff model. The puff model prediction based on this actual data formed the basis for the model performance evaluations carried out here. From this basis, different input variables were adjusted to note the effect on the advected concentrations--both in relation to each other and to the airborne measurements.

IV. MODEL BEHAVIOR

The Puff Model was run on the NPS IBM S/370 Model 3033 AP computer with two goals in mind; (1) familiarization with model performance under actual conditions and (2) a comparison of model predictions with observed data. The two goals are interrelated in the sense that atmospheric data collected in the aforementioned tracer study were used to form an initial prediction of the plume dispersion, and variations of that data were used to evaluate the limits of the model. The data used as input to the model represented the marine atmospheric conditions as determined from R/V Acania meteorological data at the time of the experiment.

Proper grid spacing was arrived at by considering puff spread, mean wind direction and the geographical area of interest. With the initial prediction in hand, data input variables of the model were adjusted and their effects (changes in prediction) noted. All model predictions were compared with the aircraft observed data.

A 7.4 X 4.3 km downwind area of interest was initially gridded into an 17 X 10 array. Distances between horizontal and vertical grid points were approximately 435 m (Fig. 2).

Since many of the aircraft observation times centered around 1730 hours (all times are Pacific Daylight Time), model puff releases were initiated at 1630. The 30-minute wind speed averages obtained from data taken onboard the ship between 1630 and 1730 were 4.7 and 4.8 ms^{-1} . The first advected puffs would be expected to arrive at the back edge of the grid slightly before 1700, and by 1730 a steady consistent plume would be passing through the area of the aircraft track. (The model showed, in fact, puffs leaving the back edge of the grid slightly before 30 minutes after puff release).

The average wind direction was recorded on the ship every 15 seconds. The standard deviations of the wind direction (σ) were computed as approximate one minute averages. These, in turn, were averaged over 30 minutes to correspond with the 30-minute wind speed averages. The σ values during the time of interest were 1.0 and 0.9 resulting in the very small turbulence intensity values of .0003 and .0002.

A delta Z value of 33 m was used to observe plume concentrations at the altitudes of 0, 33, 66 and 99 m above the surface. These levels were chosen for comparison with the aircraft transect altitudes of 61 and 91 m.

Fine scale vertical temperature and humidity plots were drawn based upon radiosonde soundings taken onboard the ship. The sounding taken at 1735 PDT (Figure 4) shows a shallow unstable layer near the surface topped by an inversion extending to near 400 m. A 80 m depth of the mixing layer was subjectively established. The potential temperature gradient computed by the formula

$$\frac{\partial \theta}{\partial z} = \frac{\partial T}{\partial z} + .0098 z \quad (1)$$

was found to be 1.0 deg K/100 m.

Basic data to determine source strength and heat emission from the ships stack were taken from Schacher, et al (1981). As previously mentioned, SF_6 gas was released through the ships motor generator exhaust at a constant rate. The stack temperature was 250 deg F, the flow rate was $7.13 \times 10^3 \text{ m}^3 \text{ s}^{-1}$. The SF_6 release rate was 47.91 lb hr^{-1} . The top of the ships stack--considered to be the source elevation-- was 4 m. The source strength was converted to 6.04 gm s^{-1} for input into the model.

Heat emission (H) in KW was determined by the formula

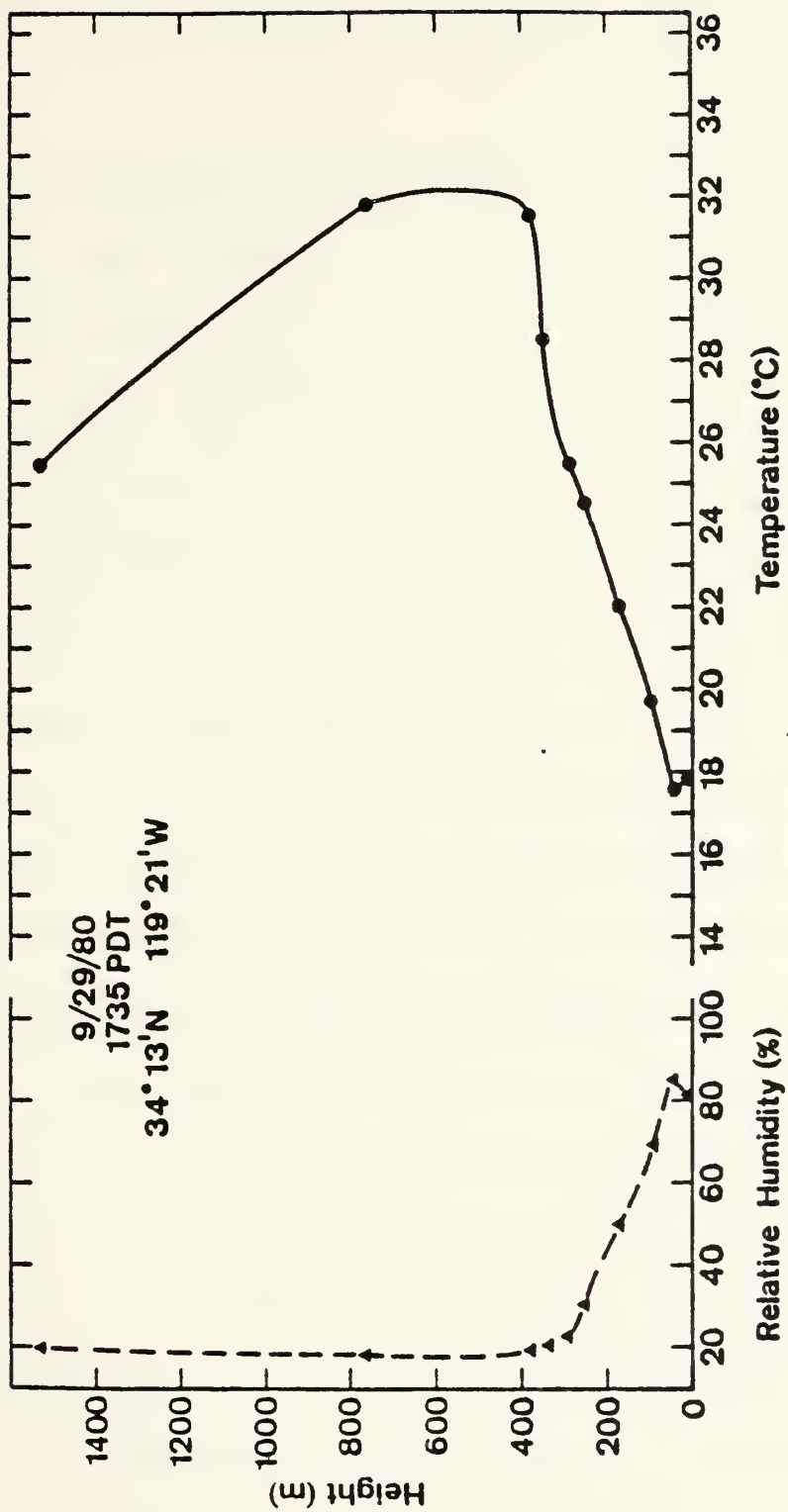


Figure 4. Radiosonde sounding taken onboard R/V Acania, 1745 PDT, September 29, 1981.

$$H = \Delta T * \frac{P}{RT} * C_p * \text{Flow} \quad (2)$$

where

delta T = temperature (stack - air) deg K

R = dry air gas constant

= 2.87×10^6 erg/g deg K

P = $10^3 * P(\text{mb})$ = dyne/cm²

C_p = specific heat of dry air

= .24 cal/g deg K

Flow = $16.39 * 7.13 * 10^3$ cm³/s

The heat emission was thus computed as 15.07 KW.

Initially the model grid was established after noting the area of maximum airborne sampled concentrations (between points 24 and 43 of Fig. 3) and the location of the ship. It became obvious during early model runs that, with the actual wind direction input, the model predicted plume was being advected south of the grid towards point 60 on the aircraft track. Obviously, the steering wind, as measured onboard ship, was not constant all the way to the shore. A northward turning of the plume was indeed detected several times during the experiments by the aircraft. To compensate

for this effect, the source of the plume release was moved in the model three grid spaces (1305 m) to the north so that the maximum predicted plume concentrations would pass through the areas of the maximum airborne measured concentrations. No corrections were made to the model predicted plume concentrations because of this adjustment. However, one could reason that the predicted concentration values would be higher in comparison with measured values since the coastal turbulence and wind shift--which would tend to diffuse the plume--were not considered.

Initial model runs with the small turbulence intensity classifications of .0003 and .0002 failed to show plume concentrations greater than 1×10^{-12} in the grid at any level other than at the source. Apparently, the grid spacing was too large and the narrow plume was advecting between the grid points. In an effort to locate the plume, a combination of model runs were performed varying the turbulence intensity and grid spacing as shown in Table I.

In this table, a mixing level cap of 80 m was in effect for the model predictions. No concentrations above that level were allowed in the computations. As previously mentioned, the model mixing level cap totally reflects all pollutants back downward.

TABLE I. A Comparison of Predicted Concentrations at the Surface, 40 and 80 m at the East Edge of the Grid with Turbulence Intensities between .01 and .05. Mixing Level Limit is 80 m. $E = (*10)$. Numbers in Parenthesis are Grid Numbers along Y Axis from Table II.

Turbulence Intensity	Delta Y	(4)	(5)	(6)	(7)	Sfc 40 m 80 m
.01	108.75	.68E-10 .31E-10 .47E-11	.16E-4 .70E-5 .11E-5	.22E-4 .10E-4 .15E-5	.20E-9 .91E-10 .14E-10	
.01	217.5	(4) .69E-10 .31E-10 .47E-11	(5) .22E-4 .10E-4 .15E-5			
.01	435	(6) .69E-10 .31E-10 .47E-11				
.02	435	(6) .19E-5 .17E-5 .12E-5			(7) .56E-8 .50E-8 .37E-8	
.03	435	(6) .66E-5 .67E-5 .62E-5			(7) .48E-6 .49E-6 .45E-6	
.05	435	(5) .57E-8 .59E-8 .58E-8	(6) .72E-5 .74E-5 .72E-5		(7) .26E-5 .27E-5 .26E-5	(8) .28E-9 .29E-9 .29E-9

With a grid spacing of 435 m and a turbulence intensity of .05, a plume concentration covering four grid spaces at the east end of the grid was produced. Predicted plume concentrations slowly decreased as the turbulence intensity was reduced to .02 (atmospheric stability increased). At an intensity of .01, the concentration dropped by about five orders of magnitude. Normally, one would expect increased concentrations with increased atmospheric stability. Perhaps the result noted here is due to the plume shrinking away from a grid point (and becoming more concentrated between the recorded grids) with the increase in stability.

To increase the grid resolution, the grid spacing was reduced by half to 217.5 m and again to 108.75 m. With each reduction the grid was reduced by half in the "Y" direction and doubled in the "X" direction thus keeping distances between grid spaces equal in all directions. This of course greatly increases the computational requirements. If only plume predictions along the back edge are needed (as in Table I), the downwind grid distance may be held constant at 435 m while the horizontal crosswind resolution is increased. In this way many unnecessary computations are not made. However, the increased horizontal crosswind resolution is

computed over the entire downwind grid, which in this case, is not necessary. A more satisfying solution to this problem is to install the capability of using a variable resolution grid with the model so that downwind areas of particular interest can be covered with a dense grid while other areas of not so much interest can be sparsely grided.

In order for the advection of the plume to remain on the array when increasing the horizontal crosswind resolution and decreasing the area exposed on the grid, the plume source was adjusted along the western boundary of the grid. The relationship of the vertical grid points to changes of the source location is shown in Table II. The plume source for each grid resolution is noted with an arrowhead. Grid points that are aligned vertically in the table have identical locations and should have the same predicted plume concentrations. As mentioned earlier, an increase of grid resolution does not affect the predicted concentration. Notice that for the same grid points in Table I, the predicted concentrations with a turbulence intensity of .01 remain constant with changes in grid spacing--only the grid resolution was changed.

TABLE II

The Relationship of the Y Axis along the Western Grid Edge to changes of Grid Distance between 435 and 108.75 m.

DELTA Y (m)	Grid Points Along the Y Axis											
435	4		5		6		7		8		9	
217.5	0	1	2	3	4	5	6	7	8	9		
108.75			0	1	2	3	4	5	6	7	8	9

From Table I it is obvious that the 435 m grid spacing is too large and that the higher resolution does indeed "see" concentrations that would otherwise be missed.

The problem of an increasingly narrow distance covered on the grid as resolution is increased can sometimes be at least partly corrected by reversing the X and Y coordinates and adjusting or rotating the advecting wind direction. This can easily be done with the use of the "TURN" model input parameter. This procedure sometimes becomes necessary since one of the grid directions is limited by the width of the output printer paper to less than or equal 10 grid units.

The model input variables, meteorological and source values were adjusted to note their effect on plume concentrations. A deeper understanding of how the model works and how the atmosphere affects dispersion can also be gained by

such adjustments. A turbulence intensity class of .05 was used, except when studying intensity itself, because it had previously demonstrated a good downwind grid coverage of the plume.

In order to note the effect of the maximum mixing level on the plume concentrations, several model predictions were run, varying only the height to which the plume was allowed to rise. Exact grid point reproductions were not possible since the model only allows the height of the mixing level to be an integer multiple of ΔZ . The vertical grid spacing is therefore not equal. However, the anticipated trend of increased concentrations as the mixing level is lowered is evident from Table III.

The reflection/absorption of the plume at the surface is controlled by the model variable "REFLEC". Tests of the extremes of total absorption (0.0) and total reflection (1.0) were performed. The results showed a 50 percent reduction in plume concentrations at the west end of the grid with total absorption compared to total reflection in otherwise identical model runs.

The model has a self-imposed limitation of 100 puffs from all sources on the grid. The model will terminate if

TABLE III

Plume Concentrations between Surface and 99 m under
Different Maximum Mixing Levels.

Max Mixing Level	(5)	(6)	(7)	(8)	
None	.44E-8	.55E-5	.20E-5	.22E-9	Sfc
	.43E-8	.54E-5	.19E-5	.21E-9	33 m
	.40E-8	.50E-5	.18E-5	.20E-9	66 m
	.36E-8	.45E-5	.16E-5	.18E-9	99 m
80 m	.57E-8	.72E-5	.26E-5	.28E-9	Sfc
	.59E-8	.74E-5	.27E-5	.29E-9	40 m
	.58E-8	.72E-5	.26E-5	.29E-9	80 m
	0	0	0	0	> 80 m
30 m	.64E-8	.81E-5	.29E-5	.32E-9	Sfc
	.65E-8	.81E-5	.29E-5	.32E-9	30 m
	0	0	0	0	> 30 m

this number is exceeded. A balance must be made between the rate at which puffs are released from the source (TAU) and the time it takes the puffs to be advected across the grid. A release rate of one puff every 40 seconds was predominantly used during this study.

The turbulence intensity variable was varied to include conditions that are more unstable. As atmospheric instability increases, the plume would be expected to expand whereas, with stable conditions, the plume should remain narrow and highly concentrated.

With the use of NPS contouring routines and the subroutine "DRAW", a visual comparison of the plume disposition and concentrations is available. Since the computed plume concentration varies over many orders of magnitude, the concentration values were converted to integer numbers by multiplying by $1. \times 10^{13}$ and then taking the logarithm. These logarithms are then smoothed. Thus, a contour plot representing order of magnitude concentrations was produced. As with the model variables "MAPTIM" and "KPLANS" which control the frequency and vertical levels of printer plots, "DRAW" can be called to contour concentrations at any time period and for any level required.

Plume concentration distributions for turbulence intensities of .05, .10 and .25, all other variables constant, are shown in Figs. 5, 6 and 7. As expected, the plume becomes wider and the concentration decreases as the turbulence intensity/diffusion increases and the atmosphere becomes less stable.

In Figs. 5-7, the plume source was located at grid point (0,6). The wide plume in the lower part of the plot is not real but is a function of the smoothing routine spreading the early puffs more than would be expected. Since the

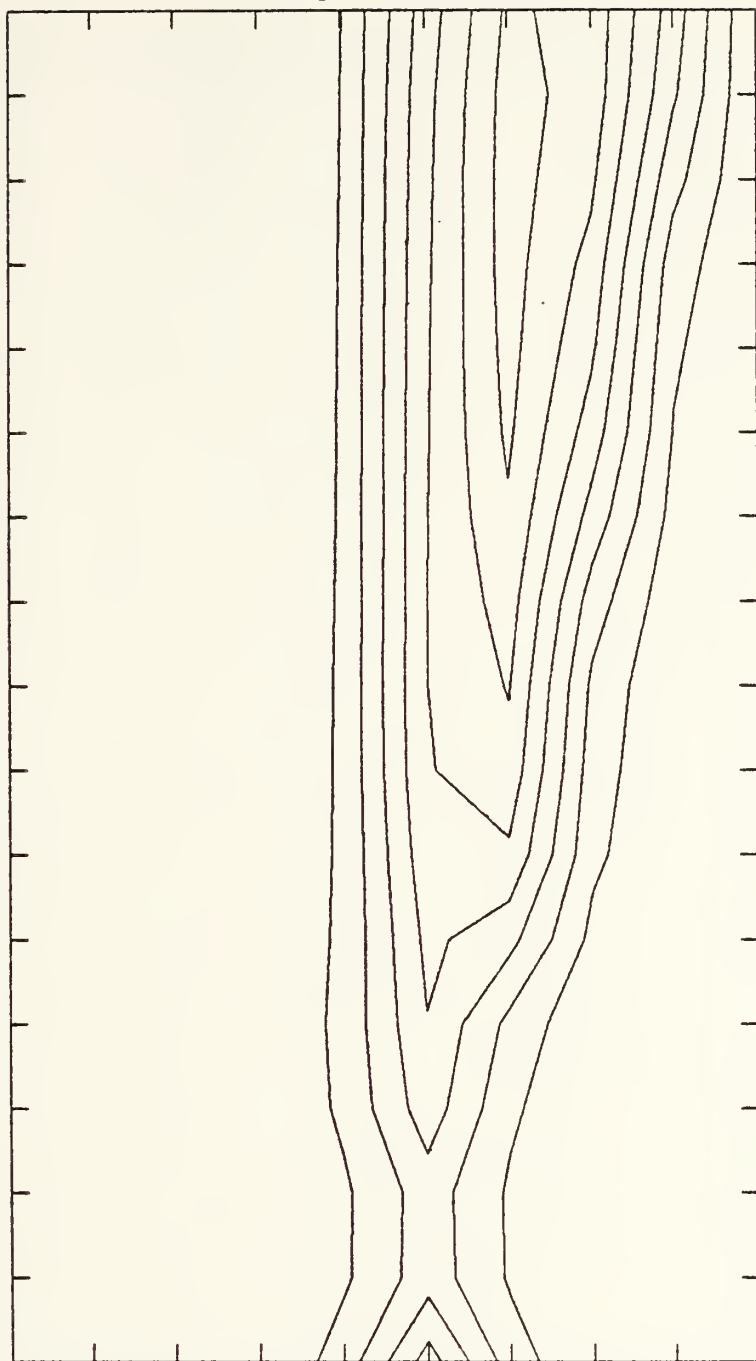


Figure 5. Orders of Magnitude of Plume Concentration with Turbulence Intensity equal to .05.

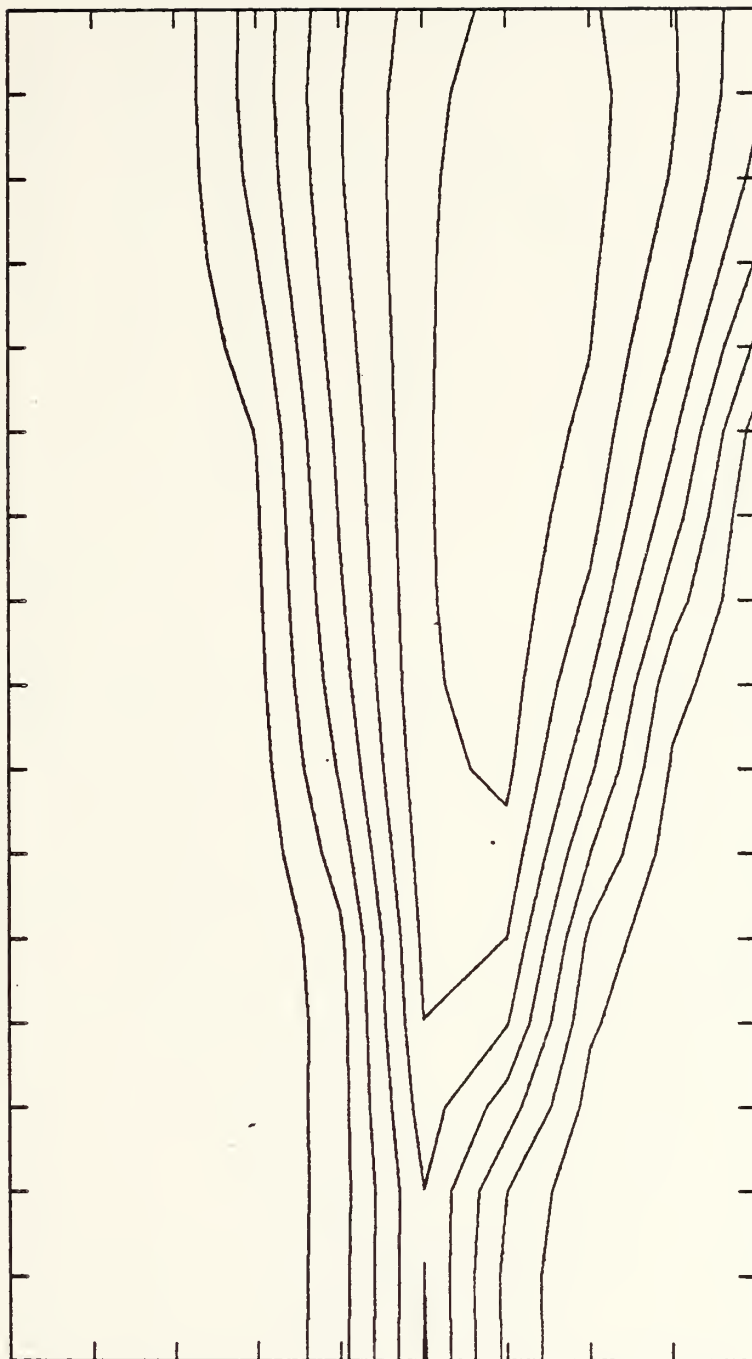


Figure 6. Same as Figure 5 except Turbulence Intensity equal to .10.

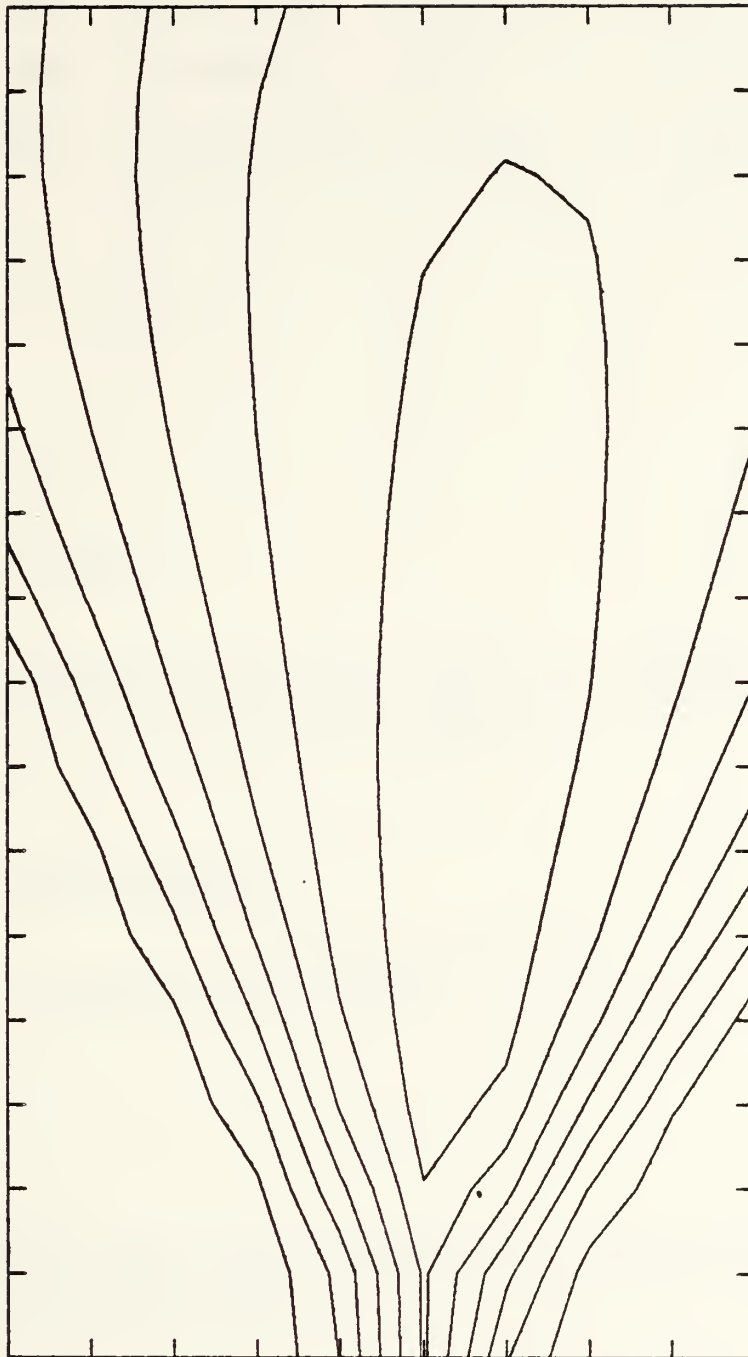


Figure 7. Same as Figure 5 except Turbulence Intensity equal to .25.

smoothing routine would tend to smooth strong concentrations near the source, the smoothing should be eliminated if the primary interest is near the source. Actually one would expect the puffs to behave as in Fig. 8, from Mikkelsen (1979), showing the relationship between the puff size and concentration, the rate of puff release (τ) and the advecting wind speed U .

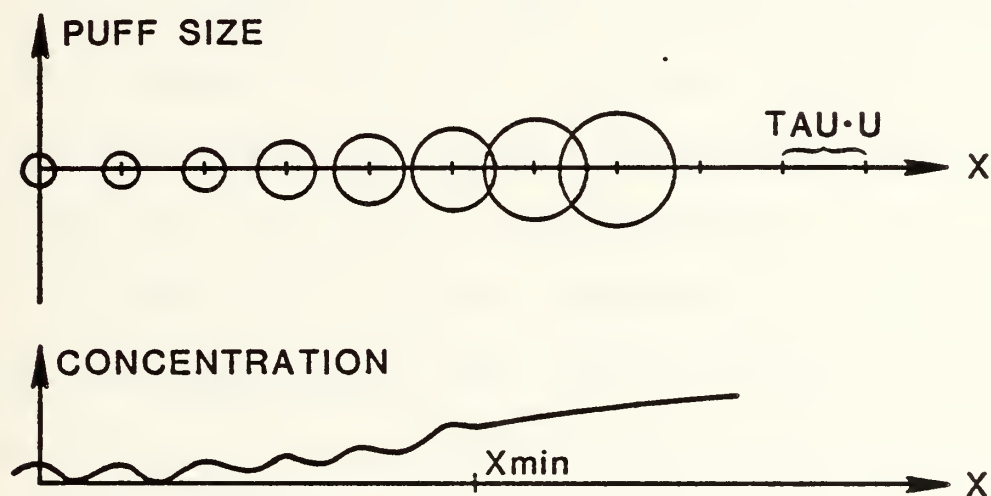


Figure 8. Relationship between Puff Size, Concentration, Puff Release Rate (τ) and Advecting Wind Speed U (Mikkelsen, 1979).

puffs would have to travel the distance X_{min} before they expand to a size where they effectively overlap and form a solid plume. From Figs. 5-7, one can see that plume concentrations have increased with distance and that a X_{min} has been reached in the middle to upper part of the grid. It is at this point that the puff model would be expected to accurately predict plume concentrations. If the area of interest is before the present X_{min} , the release rate of puffs would need to be increased so that the successive puffs would overlap sooner. Also noted that as the turbulence intensity increases, the area of maximum concentration of the plume expands while the central concentration decreases. This agrees with conservation of mass theory.

To appreciate the relative importance of the source strength and buoyant heat flux, these variables (discussed in Chapter IV) were doubled separately and together and the concentrations compared to the concentrations from the actual conditions. Little or no changes in concentration were noted when the buoyant heat flux was doubled and source strength remained the same. However, when the source strength was doubled and heat flux held constant, the grid concentrations doubled as expected. Thus, under existing

conditions, the source strength was critical to the predicted plume concentrations while the buoyant heat flux, within the range tested, was not relevant. The vertical printer plots did show an initial puff rise soon after release due to the initial heat release but as the puff rose and expanded, it soon reached the ambient temperature and leveled off. The buoyant heat flux would probably be more important when dealing with a smaller scale grid or greater heat release.

V. DATA COMPARISON

No attempt was made to compare actual puff model concentration predictions at exact grid points to aircraft observations for the following reasons:

- The aircraft locations were approximations--the exact locations were not known. Large differences in predicted concentrations are seen with small grid separations as evidenced in Table II.
- As noted in Fig. 2, the aircraft observations were taken over a period of time at different levels--while the puff model produced multilevel instantaneous predictions.
- As mentioned earlier, the actual wind was not constant between the ship observation site and the oppsite side of the grid near shore. Since the model advects the puffs based upon ship observed wind, the behavior of actual plume would be different from predicted.
- Calabration procedures for the SF₆ continuous analyzer mounted onboard the aircraft were not available for instantaneous concentrations greater than 1010 PPT.

Therefore, a question of actual levels of SF_6

concentration in the higher ranges exists.

The puff model predicted concentrations are expressed in g/m^3 while the aircraft observations are shown as the volume of SF_6 per unit volume of air in PPT. A conversion between the predicted and observed concentrations was obtained by computing the partial pressure and molecular weight of SF_6 at standard pressure and temperature. A conversion of

$$\text{g}/\text{m}^3 = (.63 \times 10^{-11}) * \text{observed concentration (PPT)}$$

was thus found.

Generally, the aircraft sampled concentrations (Fig. 2) show values between 100 and 8000 PPT. Converting these observed concentrations to predicted concentration units gives values between $.63 \times 10^{-9}$ and $.50 \times 10^{-7} \text{ g}/\text{m}^3$. These observed concentrations are much smaller than the values shown in Table II. Perhaps this difference could be explained by the fact that the puff model advected the plume toward the coast in the same direction under the same very stable conditions as observed on the ship. Any consideration of increased turbulence and wind shifts near shore would be expected to reduce the actual plume concentrations toward the observed concentration levels.

Increasing the turbulence intensity to 0.25 and keeping all other variables constant, the concentration values would decrease to the order of magnitude of 10^{-6} --closer to the observed concentrations. (This would require the wind direction standard deviation to increase from 1 to 28). However the increased instability would cause the plume to spread over a much greater area (Fig. 7) than observed by the aircraft.

VI. CONCLUSIONS AND RECOMMENDATIONS

The puff model has been demonstrated to be a versatile working dispersion model. Different combinations of input variables showed the expected reasonable results. The differences between model predicted and aircraft observed plume concentrations do not seem to be the fault of the model but mainly that of the highly variable meteorological conditions found along a coast.

Probably the most obvious conclusion reached from this study is that predicting the behavior of a plume moving over a marine environment onto a coastal region has significant problems. In all probability, atmospheric boundary layer conditions 7.4 km offshore can be very different from those observed in the more turbulent coastal region. The single point meteorological measurement at the source should not be expected to adequately represent plume characteristics as it nears a meteorologically variable coastline. Additional observations (primarily wind speed and direction), or other means of predicting the coastal meteorological conditions, would have to be incorporated into the puff model to adequately handle this problem.

The advantage of incorporating variable grid spacing within the puff model and the obvious benefits have already been discussed.

Presently, the mixing cap of the puff model is required to be located at an integer multiple of ΔZ . More flexibility in this parameter to include any level, regardless of ΔZ , would be beneficial.

Along with the puff locations shown on the lineprinter output, a maximum concentration level of each puff would be helpful.

In future experiments, several aircraft tracks should be made further out from the coast in an attempt to avoid the turbulent coastal region. Observations thus obtained in a noncoastal environment would help to verify the model predictions without the coastal influence.

APPENDIX A

MAJOR SECTIONS OF THE PUFF MODEL

The Risø Puff Model has been described by (Mikkelsen, 1979). The code also is well documented with comment statements. With that information and the outline to be provided in this and the following appendices, the computational and input/output procedures will be obvious.

The program and input data are stored on cards for the sake of permanency. For efficient operational execution, the program and input data cards are read on a disk within the computer. The model can then be run at will without reference to the original data cards. Minor changes can easily be made directly on the disk both to the model and/or data before each execution.

The model can be separated into the following main sections:

- A. Input Data
- B. Initial
- C. Calculating
- D. Output
- E. Error Diagnostics
- F. Subroutines

These will be described separately in the following sections.

A. INPUT DATA SECTION

The input data includes the variables shown in Table IV.

TABLE IV

Input Data Variables for the Puff Dispersion Model.

Wind History	Potential Temperature Gradient
Turbulence Intensity	Buoyant Heat Flux
Grid Dimensions	Minimum Concentration of Interest
Mixing Depth	Reflection at Ground Level
Source Locations, Start/Stop Time, Strength, Heat Emission	
Number of Seconds between Advection Steps	
Number of Seconds between Printouts/Plots	
Number of Seconds between Puff Releases	

The wind field and stability class for the current time step are read at the start of the calculation section.

The variables listed above are printed as a input data check and a permanent record to accompany the actual output. In most cases the print command can be overridden by YES/NO options.

B. INITIAL SECTION

Based upon the input data from section (A), the initial section specifies and initializes parameters to be used in

the calculating section and is passed only once during execution of the model. The grid and some counters are initialized. Constants relating to reflectance, mixing depth and stability as well as those controlling the size of some of the loops within the model are established. Parameters such as number of puff releases per second, number of advection steps per second and number of advection steps per puff release are determined.

C. CALCULATION SECTION

Using current wind and stability class data read at the start of the calculation section, the model advects the puff centers and calculates the growth rate and plume rise of the puffs. It removes the puffs that have left the grid (horizontally and/or vertically). The predicted concentration is computed at the grid points to include pollutants from all nearby puffs.

D. OUTPUT SECTION

For time intervals designated by the input data, printer plots of the X-Y and Y-Z grid are produced. A maximum mixing level is marked on the Y-Z grid if in effect.

These plots include the source location and a trace of the plume from the release time to the maptime. Also printed at this interval is a X-Y table of grid concentrations for each vertical level of interest. These concentrations can be either accumulated or actual concentrations at the plot time.

Added to the puff model is a versatic plotter routine to smooth and contour the grid magnitude concentrations of the above tables.

E. ERROR DIAGNOSTIC SECTION

If the model is directed by the input data beyond the limits of the design of the program, the program is terminated by way of the error diagnostic section. It prints comments relating to commonly made input errors enabling the user to isolate problems.

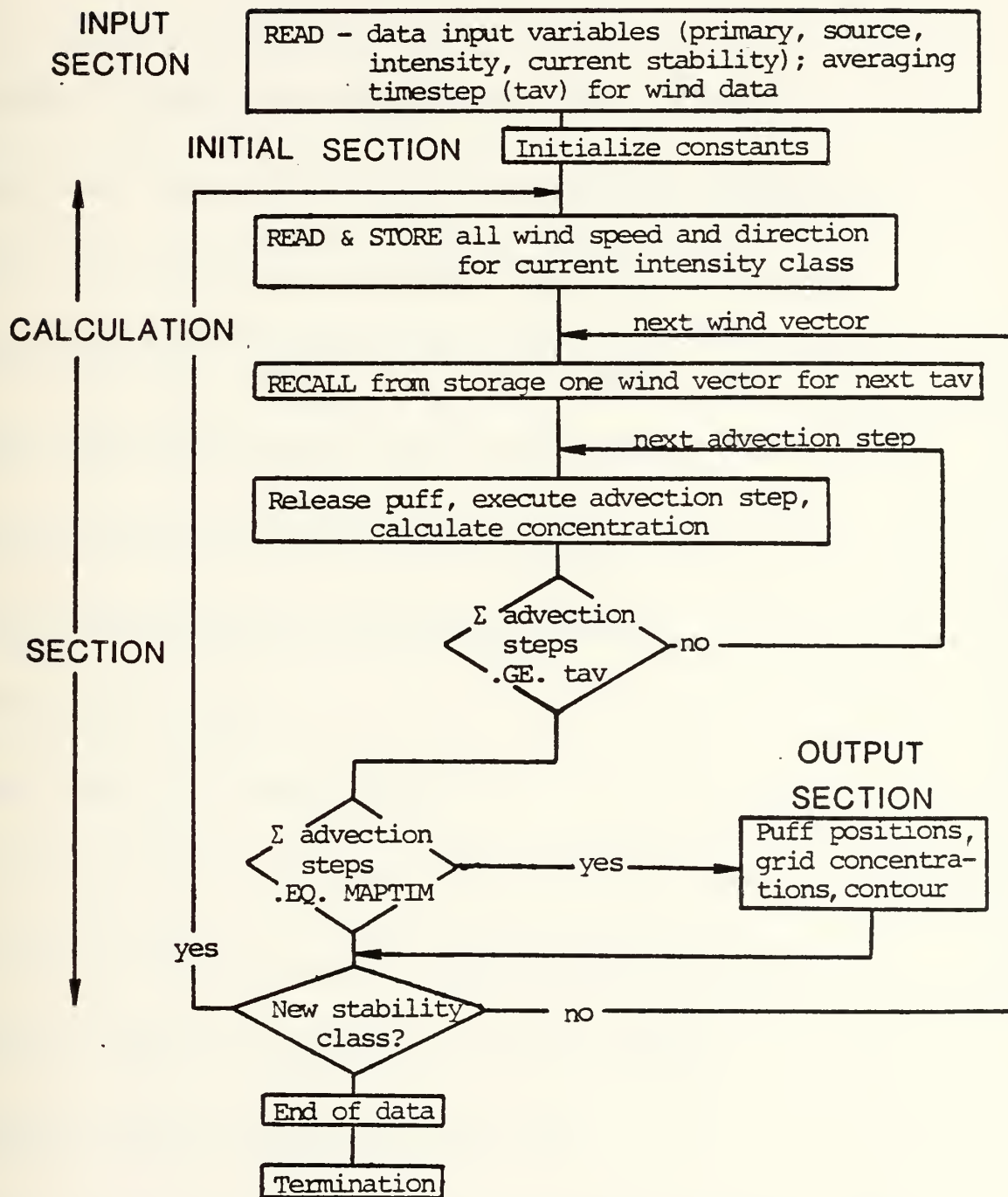
F. SUBROUTINES

The subroutine "Sigris" calculates the puff size in the horizontal and vertical directions. It also estimates plume rise associated with pollutent buoyancy.

The subroutines "Ispace" and "Rspace" are used in the framework of the printer plots.

The subroutine "Draw" converts the plume concentrations to a logarithmic values, smoothes and then contours them using NPS inhouse contour subroutines. The values are converted to their logarithm values so that the problem of contouring over many orders of magnitude is simplified.

APPENDIX B
PUFF MODEL FLOW CHART



APPENDIX C

PUFF MODEL CONTRACTIONS

CHEMIN--Minimum grid concentration of interest

DELX,DELY,DELZ--Distance in meters between grid points

DOSE--Allows the concentration matrix to accumulate

DTDZ--Potential temperature gradient (K/M) (.GE. 0)

HEAT--Individual source heat emission (KW)

ICOLS--Number of columns in grid (.LE. 10)

INST--Instantaneous concentration matrix

ITIME--Start time

JROWS--Number of rows in grid

KPLANS--Number of vertical levels in grid (includes surface)

MAPTIM--Number of seconds between printer plots

NRELSE--Number of seconds to stop of release

NRMULT--Number of sources (.LE. 25)

NTADV--Integer number of seconds between advection steps

REFLEC--Reflection at ground level (0. none;1.0 total)

SOURNR--Number to identify source

SOURST--Strength for individual source (gm/s)

STOPRL--Individual source stop time (s)

STRTRL--Individual source start time (s)

TAU--Integer number of seconds between puff releases

TURN--Angle of rotation of wind direction

XSOURCE--X coordinate of source in grid units

YSOURCE--Y coordinate of source in grid units

ZM--Limited mixing depth (m)

LISTING OF PUFF MODEL COMPUTER CODE

```

DIMENSION STRING(105), HORFIRM(105), VERFIRM(105), -RFRMZ(105), VRFRMZ(
105), VERPLS(105), VRPLSZ(105), PARENT(105), NBUF(7), SBUF(7)
REAL BL1, SN1/*, SN2/*, SN3/*+, SN4/*-, SN5/*, SN6/*,

```

PUF 00410
PUF 00420
PUF 00430
PUF 00440


```

600 FORMAT(6X,8HDELX      =,F10.2,6X,8HDELY      =,F10.2,6X,8HDELZ      =,F10.2
1) PUF00960
700 FORMAT(6X,8HCHEMIN    =,E10.4,6X,8HREFLEC    =,F10.5,6X,13HTURN      =
1) PUF00970
C 1 SKIPPING LINE PRINTING OF PRIMDATA IF SPECIFIED PUF00980
IF(ABC(5) .EQ. NO ) GO TO 751 PUF00990
DO 750 I = 1,5 PUF01000
750 WRITE(6,1) PUF01010
WRITE(6,35) TITLE PUF01020
WRITE(6,1) PUF01030
WRITE(6,1) PUF01040
WRITE(6,1) PUF01050
WRITE(6,1) PUF01060
WRITE(6,1) PUF01070
WRITE(6,1) PUF01080
WRITE(6,1) PUF01090
WRITE(6,1) PUF01100
WRITE(6,1) PUF01110
WRITE(6,1) PUF01120
WRITE(6,1) PUF01130
WRITE(6,1) PUF01140
WRITE(6,1) PUF01150
WRITE(6,600) DELX,DELY,DELZ PUF01160
WRITE(6,1) PUF01170
WRITE(6,700) CHEMIN,REFLEC,TURN PUF01180
WRITE(6,1) PUF01190
C 751 CONTINUE PUF01200
C READ SOURCEDATA INPUT FILE PUF01210
C PUF01230
C PUF01240
C PUF01250
800 FORMAT(A1,I2,A1) PUF01260
810 FORMAT(5I5,3F10.5) PUF01270
820 FORMAT(48H CURRENT SOURCEDATA : NUMBER OF ACTIVE SOURCES :,I4) PUF01280
C PUF01290
C PUF01300
C PUF01310
C PUF01320
C PUF01330
C PUF01340
C PUF01350
C PUF01360
C PUF01370
C PUF01380
C PUF01390
C PUF01400
C PUF01410
C PUF01420

```



```

C      OUTPRINTING CURRENT SOURCE POSITION(S) IN GRID PICTURE
C
C      SKIP PLOT OF SOURCE POSITIONS IF SPECIFIED IN 'RIMDA
C      IF(ABC(6) .EQ. NO ) GO TO 999
C
C      IF(ICOLS.GT. 10) GO TO 995
860  FORMAT(1H ,49X,33H CURRENT SOURCE DATA AS SPECIFIED,/50X,27H IN SOURCE
865  1 SOURCE DATA INPUT FILE:,//)
865  1 FORMAT(1H0,50X,'SOURCES ARE REPRESENTED BY:','/55X,'SOURCE NUMBER',
1/55X,'START TIME (SEC)',/55X,'STOP TIME (SEC)',/55X,
2,'SOURCE STRENGTH',/55X,'BUOYANT HEAT FLUX.://')
C
870  FORMAT(2H0 ,16H Y COORDINATE OF,25X,32H X COORDINATE OF THE GRID P
10INTS/2X,16H THE GRID POINTS,18,9110/)
871  FORMAT(2H0 ,16H Y COORDINATE OF,25X,32H Z COORDINATE OF THE GRID P
10INTS/2X,16H THE GRID POINTS,18,9110/)
C
C      WRITE(6,860)
C      WRITE(6,865)
C      WRITE(6,870) (I,I=XS,XLB)
C      WRITING DATA INTO GRIDPOINTS:
910  FORMAT(1H+ ,11,5X,2H +,105A1)
912  FORMAT(1H+ ,19X,105A1)
913  FORMAT(1H ,17X,1H,105A1/1H ,17X,1H,105A1)
914  FORMAT(1H+ ,17X,1H,105A1)
C
C      WRITE(6,1)
C      WRITE(6,912) HORFRM
C      WRITE(6,913) VERFRM,VERFRM
C      MAX =JROWS -1
C      NY5=MAX+1
C      DO 950 NY6=1,NY5
C      I=NY6-1
C      MAXMI = MAX - I
C      WRITE(6,910) MAXMI, VERPLS
C      DO 920 J=1,NRMULT
C      IF(MAX-I .NE. YSOURC(J) ) GO TO 920
C      CALL ISPACE(XSOURC(J),J)
C      CONTINUE
920  WRITE(6,913) VERFRM,VERFRM
C
C      DO 932 J = 1,NRMULT
C      IF(MAX-I .NE.YSOURC(J)) GO TO 932
C      WRITE(6,914) VERFRM
C      CALL ISPACE(XSOURC(J),STRRL(J))
C      CONTINUE
932  WRITE(6,913) VERFRM,VERFRM

```

PUF01920
 PUF01930
 PUF01940
 PUF01950
 PUF01970
 PUF01980
 PUF01990
 PUF02000
 PUF02010
 PUF02050
 PUF02060
 PUF02070
 PUF02080
 PUF02090
 PUF02100
 PUF02110
 PUF02120
 PUF02130
 PUF02140
 PUF02150
 PUF02160
 PUF02170
 PUF02190
 PUF02200
 PUF02210
 PUF02220
 PUF02230
 PUF02240
 PUF02250
 PUF02260
 PUF02270
 PUF02280
 PUF02290
 PUF02300
 PUF02310
 PUF02320
 PUF02330
 PUF02340
 PUF02350
 PUF02360
 PUF02370
 PUF02380
 PUF02390
 PUF02400
 PUF02410


```

C          DO 934 J = 1,NRMULT
          IF(MAX-I.NE.YSOURC(J)) GO TO 934
          WRITE(6,914) VERFRM
          CALL ISPACE(XSOURC(J),STOPRL(J))
          CONTINUE
934        WRITE(6,913) VERFRM,VERFRM
C
          DO 940 J=1,NRMULT
          IF(MAX-I.NE.YSOURC(J) ) GO TO 940
          WRITE(6,914) VERFRM
          CALL RSPACE(XSOURC(J),SOURST(J))
          CONTINUE
940        WRITE(6,913) VERFRM,VERFRM
C
          DO 930 J=1,NRMULT
          IF(MAX-I.NE.YSOURC(J) ) GO TO 930
          WRITE(6,914) VERFRM
          CALL RSPACE(XSOURC(J),HEATFX(J))
          CONTINUE
930        WRITE(6,913) VERFRM,VERFRM
          WRITE(6,913) VERFRM,VERFRM
C
          CONTINUE
          WRITE(6,1)
          WRITE(6,912) HORFRM
C
          GO TO 999
990        FORMAT(53H SOURCE DATA PLOT SUPPRESSED BECAUSE" ICOLS"EXCEEDS 10)
995        WRITE(6,990)
999        CONTINUE
C
          DEFINE STABILITY AND INTENSITY CLASSES
          INPUT FROM INTENSITY - DATA: INTSDA
C
          960 FORMAT(14 F5.4)
          965 FORMAT(1H0, 46H IN THE CURRENT RUN, THE STABILITY-CLASSES ARE,/41H
          1 CONNECTED TO INTENSITY DATA AS FOLLOWS:)
          970 FORMAT(1H ,21H STABILITY CLASS NO. :,I3,I3I5)
          975 FORMAT(1H ,21H INTENSITY DATA :, 14F5.4)
C
          READ INTSDA,TITLE-STRING:
          READ(5,30) INSTX
          WRITE(6,30) INSTX
          READ INTSDA, NO. OF INTENSITY-CLASSES: NRINCL
          READ(5,800) ABC(3),NRINCL,ABC(4)
          WRITE(6,802) NRINCL
          INPUT FORMAT TESTING:
          PUF02420
          PUF02430
          PUF02440
          PUF02450
          PUF02460
          PUF02470
          PUF02480
          PUF02490
          PUF02500
          PUF02510
          PUF02520
          PUF02530
          PUF02540
          PUF02550
          PUF02560
          PUF02570
          PUF02580
          PUF02590
          PUF02600
          PUF02610
          PUF02620
          PUF02630
          PUF02640
          PUF02660
          PUF02670
          PUF02680
          PUF02700
          PUF02710
          PUF02720
          PUF02730
          PUF02740
          PUF02750
          PUF02760
          PUF02770
          PUF02780
          PUF02790
          PUF02800
          PUF02810
          PUF02820
          PUF02830
          PUF02840
          PUF02850
          PUF02870
          PUF02880
          PUF02890

```



```

802 FORMAT(1X,I5)
C IF(ABC(3).NE.AA.OR.ABC(4).NE.AA) GO TO 8890
C READ IN INTENSITY-CLASSES INTO REAL ARRAY: INTENS
C READ(5,960,END=801) (INTENS(I),I=1,NRINCL)
C WRITE(6,960) (INTENS(I),I=1,NRINCL)
C
C OUTPRINTING CURRENT INTENSITY CLASSES:
C
C SKIP PRINTING OF INTENSITY DATA IF SPECIFIED IN PRIMDA
801 IF(ABC(7).EQ.NO) GO TO 980
C WRITE(6,2)
C WRITE(6,35) INTSTX
C WRITE(6,1)
C WRITE(6,965)
C WRITE(6,970) (I,I=1,NRINCL)
C WRITE(6,975) (INTENS(I),I=1,NRINCL)
C WRITE(6,1)
C WRITE(6,1)
C CONTINUE
C
C 980
C END OF INTENSITY DATA SECTION.
C
C INPUT FROM STABILITY DATA:STABDA
C
C READ STABDA,IITLESTRING:
C READ(3,30) STABTX
C READ(3,STABDA,POTENTIAL TEMPERATURE GRADIENT (>0).
C READ(3,889) DT0Z
C READ(3,STABDA,LIMIT OF MIXING DEPTH: ZM (METERS).
C READ(3,992) ZM
C INDATA-TEST ON ZM:
C IF(AMOD(ZM,DELZ).NE.0.)GO TO 8880
C
C OUTPRINTING CURRENT STABILITY-DATA:
C
C 889 FORMAT(F10.4)
C 991 FORMAT(1H0,45H IN THE CURRENT RUN,THE POTENTIAL TEMPERATURE/21H
C 992 1RADIANT IS SET TO:,F10.4)
C 993 FORMAT(F10.2)
C 994 FORMAT(1H0,36H NO FINAL MIXING DEPTH IS SPECIFIED.)
C
C FORMAT(1H0,32H THE MIXING LAYER IS LIMITED AT:,F10.2,8H METERS.)
C WRITE(6,1)
C WRITE(6,1)
C WRITE(6,1) STABTX
C WRITE(6,35)
C WRITE(6,1)
C WRITE(6,1)
C WRITE(6,991) DTDZ
C WRITE(6,1)

```

PUF02900
 PUF02910
 PUF02920

 PUF02930
 PUF02940
 PUF02950

 PUF02970
 PUF02980
 PUF02990
 PUF03000
 PUF03010
 PUF03020
 PUF03030
 PUF03040
 PUF03050
 PUF03060
 PUF03070
 PUF03080
 PUF03100
 PUF03110

 PUF03120

 PUF03140
 PUF03150
 PUF03160
 PUF03170
 PUF03180

 PUF03200
 PUF03210
 PUF03220
 PUF03230
 PUF03240
 PUF03250
 PUF03260
 PUF03270
 PUF03280
 PUF03290
 PUF03300
 PUF03310
 PUF03320
 PUF03330
 PUF03340
 PUF03350


```

C      WRITE(6,1)
C      IF(ZM.EQ. 0.) WRITE(6,993)
C      IF(ZM.GT. 0.) WRITE(6,994) ZM
C
C      END OF STABILITY DATA SECTION.
C
C      INPUT FROM WINDDATA:
C      1110 FORMAT(16,1X,14,1X,1A1,14,1A1)
C      1120 FORMAT(1H0,28HCURRENT WINDDATA: STARTDATE=,16,4X,10HSTARTHOUR=,14,
C      14X,14HWINDAV.(SEC.)=,14)
C      READ WINDDA,TITLE STRING:
C      READ(2,30) WINDTX
C      READ WINDDA, STARTTIME AND WINDFIELD AVERAGING TIME:
C      READ(2,110) DATE,STRTHR,ABC(1),WINDAV,ABC(2)
C      INPUT FORMAT TESTING:
C      IF(ABC(1).NE.AA.OR.ABC(2).NE.AA) GO TO 8990
C      WRITE(6,2)
C      WRITE(6,1)
C      WRITE(6,1)
C      WRITE(6,1)
C      WRITE(6,35) WINDTX
C      WRITE(6,1)
C      WRITE(6,1120) DATE,STRTHR,WINDAV
C
C      TESTING ON SPECIFIED TIME INCREMENTS: TAU,NTADV,WINDAV:
C      ITEST1 = MOD(TAU,NTADV)
C      IF(ITEST1.NE.0) GO TO 8980
C      ITEST2 = MOD(WINDAV,NTADV)
C      IF(ITEST2.NE.0) GO TO 8970
C      END OF FIXED WINDDATA SPECIFICATIONS.
C
C      *****
C      *****INITIAL SECTION*****
C      *****
C      *****
C      (THIS PART OF THE PROGRAM IS ONLY PASSED ONCE.)
C
C      1130 FORMAT( 14(A1,A4))
C      COUNTER FOR STABILITY SPECIFICATIONS GIVEN BY WINDDATA: NRSTAB
C      NRSTAB=0
C      INITIATING A THREE DIMENSIONAL GRID: CHI
C      DO 1200 I = 1,ICOLS
C      DO 1200 J = 1,JROWS
C      DO 1200 K = 1,KPLANS
C      CHI(I,J,K) = 0
C
C      1200 CHI(I,J,K) = 0
C
C      PUF03360
C      PUF03370
C      PUF03380
C      PUF03390
C      PUF03400
C      PUF03410
C      PUF03420
C      PUF03440
C      PUF03450
C      PUF03460
C      PUF03470
C
C      PUF03490
C      PUF03500
C      PUF03510
C      PUF03520
C      PUF03530
C      PUF03540
C      PUF03550
C      PUF03560
C      PUF03570
C      PUF03580
C      PUF03590
C      PUF03600
C      PUF03610
C      PUF03620
C      PUF03630
C      PUF03640
C      PUF03650
C      PUF03660
C      PUF03670
C      PUF03680
C      PUF03700
C      PUF03710
C      PUF03720
C      PUF03730
C      PUF03740
C      PUF03750
C      PUF03760
C      PUF03770
C      PUF03780
C
C      PUF03800
C      PUF03810
C      PUF03820
C      PUF03830
C      PUF03840
C      PUF03850

```



```

C      NUMBER OF PUFF RELEASES PER SEC: TAUINVERS.
      TAUINV = 1.0/ FLOAT(TAU)
C
C      NUMBER OF ADVECTION STEPS PER SEC.: ADSTPS.
      ADSTPS = 1.0/ FLOAT(NTADV)
C      BASIC DOSE PER PUFF:(GRAM/SEC.)*TAU = GRAM/PJFF.
      BADOPP = 1*TAU
C
C      NUMBER OF BASIC ADVECTION STEPS (INTEGER NUMBER) PER PUFF RELEASE:
      NADPRP = TAU/NTADV
C
C      NUMBER OF BASIC ADVECTION STEPS (INTEGER NUMBER) PER WINDFIELDSP.
      NADPRW= WINDAV/NTADV
C
C
C      TOTAL RUNTIME COUNTER: TOTTIM.
      TOTTIM =0
C
C      COUNTER FOR REMOVED PUFFS: LEAVE
      LEAVE = 0
C      STABILITY PARAMETER FOR PLUMERISE:
      STABPA = G/T*(DTHETE/DZ)
C      STABPA = .033*DTDZ
C      CONSTANT IN CONNECTION WITH PLUMERISE FORMULA =OR USE IN
      SUBROUTINE SIGRIS: CONST1.
      CONST1 = 0.6667 * 1.6**1.5
C
C      IF MIXING DEPTH IS NOT SPECIFIED, SET NOMXDP = .TRUE.
      IF(ZM .EQ. 0.) NOMXDP = .TRUE.
C
C      IF REFLECTANCE AT GROUND LEVEL IS SPECIFIED, SET GRRFLX = .TRUE.
      IF(REFLEC.GT. 0.) GRRFLX = .TRUE.
C      MIXING DEPTH IN GRID-UNITS: ZMG
      ZMG = ZM/DELZ
C      TESTING THAT MIXING DEPTH IS INSIDE GRID:
      IF(ZMG.GT. (KPLANS -1)) GO TO 8870
C
C      END OF INITIAL SECTION
C
C      *****
C      *****CALCULATION SECTION*****
C      *****
C      *****
C      1135 READ (2,1130) ( TYPE(I),DATA(I) , I = 1,14)
C      READING STABILITY CLASS AND WINDDATA FROM INPUTFILE:

```

```

PUF03860
PUF03870
PUF03880
PUF03890
PUF03900
PUF03910
PUF03920
PUF03930
PUF03940
PUF03950
PUF03960
PUF03970
PUF03980
PUF03990
PUF04000
PUF04010
PUF04020
PUF04030
PUF04040
PUF04050
PUF04060
PUF04070
PUF04080
PUF04090
PUF04100
PUF04110
PUF04120
PUF04130
PUF04140

PUF04160
PUF04170

PUF04190

PUF04210
PUF04220
PUF04230
PUF04240
PUF04250
PUF04260
PUF04270
PUF04280
PUF04290
PUF04300
PUF04310
PUF04320
PUF04330

```



```

BACKSPACE 2
IF(TYPE(1).EQ.ANFO) READ(2,1131)(NBUF(1),SBUF(1),I=1,7)
IF(TYPE(1).EQ.ANFO) WRITE(6,1131)(NBUF(1),SBUF(1),I=1,7)
IF(TYPE(1).EQ.SLASH) READ(2,1130)
FORMAT(7(1X,I4,1X,F4.1))
1131 LOOP THRU WINDDATA AT SPECIFIED TIMESTEPS
C
I = 1
IF(TYPE(1).NE.SLASH) GO TO 1150
NRSTAB = NRSTAB + 1
C
COUNTING NUMBER OF WINDDATA SPECIFICATIONS: IWDASP
C
IWDASP = 0
READING STABILITY CATEGORY FROM WINDDATA:
CLASS = DATA(1)
IF(CLASS.EQ. A ) POINT = 1
IF(CLASS.EQ. B ) POINT = 2
IF(CLASS.EQ. C ) POINT = 3
IF(CLASS.EQ. D ) POINT = 4
IF(CLASS.EQ. E ) POINT = 5
IF(CLASS.EQ. PUNK) GO TO 8930
IF(CLASS.EQ. BLANK) GO TO 8940
1140 FORMAT(53H PROGRAM STOPPED ORDINARILY FM WINDDATA SPECIFICATION)
WRITE(6,1)
WRITE(6,1141) NRSTAB,POINT
C
1141 WRITE(6,1)
FORMAT(4H THE,I3,38H. STABILITY SPECIFICATION :LASS IS NO.,I1)
GO TO 1135
C
INPUT STRUCTURE TEST:
1150 IF(TYPE(1).NE.ANFO .OR. TYPE(I+1).NE.ASTER) GO TO 1160
C
IWDASP = IWDASP + 1
CURRENT WINDDATA:
JI=(I+1)/2
ANGLE=NBUF(JI)
SPEED=SBUF(JI)
GO TO 1175
1160 IF(TYPE(1).NE.BLANK .OR. TYPE(I+1).NE.BLANK) GO TO 8950
C
READ NEW DATA IN LINE 1135
GO TO 1135
1175 INDATA PART OF PROGRAM TERMINATED.
CONTINUE
C
CURRENT WINDDATA PRESENT.
C
OUTPRINTING CURRENT WINDDATA:
WRITE(6,1161) IWDASP ,ANGLE, SPEED
C

```

PUF04350
 PUF04360
 PUF04370
 PUF04380
 PUF04390
 PUF04400
 PUF04410
 PUF04420
 PUF04430
 PUF04440
 PUF04450
 PUF04460
 PUF04470
 PUF04480
 PUF04490
 PUF04500

 PUF04530
 PUF04540
 PUF04550
 PUF04560
 PUF04570
 PUF04580
 PUF04590
 PUF04600
 PUF04610
 PUF04620
 PUF04630
 PUF04640
 PUF04650
 PUF04660
 PUF04670
 PUF04680
 PUF04690
 PUF04700
 PUF04710
 PUF04720
 PUF04730
 PUF04740
 PUF04750
 PUF04760
 PUF04770
 PUF04780


```

C      CALCULATING WIND VELOCITY IN GRID UNITS: VGX, VGY
C      VGX = SPEED*(COS(ANGLE*3.142/180)) / DELX
C      VGY = SPEED*(SIN(ANGLE*3.142/180)) / DELY
C      RENAMING WIND AVERAGING TIME: WINDAV AS TAV:
C      TAV = WINDAV
C      1161 FORMAT(4H THE, I4, 49H WINDDATASET IN THE CURRENT STAB.CLASS IS: ANG
C      1LE=, I4, 8H , SPEED=, F4.1)
C      LOOP THRU BASIC ADVECTION STEPS WITH CURRENT WIND FIELD
C      DO 5000 NN=1, NADPRW
C      PUF04920
C      JUMPING OVER "ZERO-SETTING" OF CONCENTRATION MATRIX : CHI , IF
C      "DOSE MODE" IS SPECIFIED IN PRIMDA.
C      IF(ABC(8).EQ. DOSE ) GO TO 1256
C      DO 1255 IG=1, ICOLS
C      DO 1255 JG=1, JROWS
C      DO 1255 KG=1, KPLANS
C      CHI(IG, JG, KG) = 0.0
C      1255 CONTINUE
C      TIMECOUNTER: TOTTIM (SEC.)
C      TOTTIM = TOTTIM + NTADV
C      SKIPPING RELEASE-SECTION IF SPECIFIED
C      IF(TOTTIM .GT. NRELSE) GO TO 1250
C      TESTING IF RELEASE CONDITIONS ARE FULFILLED
C      IF(MOD(TOTTIM, TAU) .NE. 0) GO TO 1250
C      LOOP THRU MULTIPLE SOURCES
C      DO 1250 I2 = 1, NRMULT
C      INDIVIDUAL RELEASE CONTROL AS SPECIFIED IN SOURCE DATA:
C      IF((TOTTIM.LT. STRTRL(I2)) .OR. (TOTTIM.GT.STOPRL(I2))) GO TO 1250
C      TOTAL NUMBER RELEASED FROM SOURCE(I2): TPUFFS(I2):
C      TPUFFS(I2) = TPUFFS(I2) + 1
C      SHIFTING PUFF TABLE ONE POSITION TO THE RIGHT AND THEREBY
C      GIVING SPACE FOR ONE NEW PUFF:
C      J=1
C      1204 DO 1205 K=1, 7
C      1205 SHIFT(J+1, K) = PTABEL(I2, J, K)
C      J = J + 1

```



```

IF(J,GE,100) GO TO 8900
IF(PTABEL(I2,J,1) .NE. 0) GO TO 1204
DO 1210 L = 2,J
1209 DO 1210 K = 1,7
1210 PTABEL(I2,L,K) = SHIFT(L,K)
C
C      INSERTING NEW PUFF DATA IN PUFF TABLE AT J = 1
PTABEL(I2,1,1) = TPUFFS(I2)
C      DOSE RELEASED WITH EACH PUFF: SPECIFIED SOURCE STRENGTH*SEC.
C      BETWEEN RELEASES
PTABEL(I2,1,2) = SOURST(I2) * TAU
C
C      LOADING IN INITIAL SOURCE POSITIONS
PTABEL(I2,1,3) = XSOURC(I2)
PTABEL(I2,1,4) = YSOURC(I2)
C
C      TO AVOID NUMERICAL PROBLEMS IN ESTIMATING PLUME RISE,
C      SET SOHT(I2) (SOURCE HEIGHT) .GE. 1 METER.
PTABEL(I2,1,5) = SOHT(I2)/DELZ
C      INITIAL SIZE OF PUFFS:
C      SIGMAXY SET TO 1 METER:
PTABEL(I2,1,6) = 1
C      SIGMAZ SET TO 1 METER:
PTABEL(I2,1,7) = 1
C      END OF PUFF RELEASE SECTION.
1250 CONTINUE
C
C      ADVECTION OF ALL PUFF CENTERS
C
C      ADVANCE OF PUFF CENTERS IN GRID UNITS (HORIZONTALLY)
DGX = VGX* NTADV
DGY = VGY* NTADV
C      TOTALLY TRAVELED DISTANCE BY THE PUFFS IN METERS
C      DURING CURRENT BASIC ADVECTION STEP: DMS
DMS = SQRT((DGX*DELX)**2 + (DGY*DELY)**2)
C
C      ADVECTION SECTION FOR ALL EXISTING PUFFS:
C      LOOP THRU ALL SOURCES, COUNTING REMOVED PUFFS:LEAVE
DO 1300 I2 = 1, NRMULT
J = 1
C      SKIPPING SOURCE I2, IF THE LAST BORN PUFF HAS LEFT GRID
IF(PTABEL(I2,1,1).EQ.0) GO TO 1300
PTBL3 = PTABEL(I2,J,3) + DGX
PTBL4 = PTABEL(I2,J,4) + DGY
1260
C
C      CALLING SUBROUTINE "SIGRIS", THEREBY ADDING DEVIATION INCREMENT
C      AND PLUME RISE INCREMENT TO PUFF TABLE:

```

PUF05300
 PUF05310
 PUF05320
 PUF05330
 PUF05340
 PUF05350
 PUF05380
 PUF05390

 PUF05410
 PUF05420
 PUF05430
 PUF05440
 PUF05450
 PUF05460

PUF05500
 PUF05510
 PUF05520
 PUF05530
 PUF05540
 PUF05550
 PUF05560
 PUF05570
 PUF05580

PUF05630

 PUF05650
 PUF05660

 PUF05680
 PUF05690
 PUF05700
 PUF05720
 PUF05730
 PUF05740
 PUF05750

PUF05770
 PUF05780
 PUF05790
 PUF05800
 PUF05840
 PUF05850
 PUF05860


```

C      PTABEL(I2,J,5): Z-POSITION IN GRIDUNITS
C      PTABEL(I2,J,6): SIGMAXY IN METERS
C      PTABEL(I2,J,7): SIGMAZ IN METERS
C
C      CALL SIGRIS(PTABEL(I2,J,5),PTABEL(I2,J,6),PTABEL(I2,J,7))
C
C      INTRODUCING AN UPPER LIMIT FOR BUOYANCY CONVECTION: ZM,
C      IF(.NOT.NOMXDP.AND.PTABEL(I2,J,5).GT.ZMG) PTABEL(I2,J,5) = ZMG
C
C      Z - POSITIONS IN GRIDUNITS: PTBL5
C      PTBL5 = PTABEL(I2,J,5)
C
C      TESTING AND REMOVING PUFFS WHICH HAVE LEFT THE GRID:
C      IF(PTBL3.GT.XSB.AND.PTBL3.LT.XLB.AND.PTBL4.GT.YBB.AND.PTBL4.LE.YL
C      1L.AND.PTBL5.LT.ZLB) GO TO 1290
C
C      REMOVE SECTION
C      LEAVE = LEAVE + 1
C      IF(PTABEL(I2,J+1,1).EQ.0) GO TO 1265
C      REMOVING PUFF BORN AT SOURCE I2 WHICH IS NOT THE LONGEST LIVING:
C      LEFT JUSTIFICATION OF OLDER PUFFS:
C      JJ = J + 1
C      1269 DO 1270 K = 1,7
C      1270 SHIFT(JJ,K) = PTABEL(I2,JJ,K)
C      JJ = JJ + 1
C      IF(PTABEL(I2,JJ,1).NE.0) GO TO 1269
C      SHIFT(JJ,1) = 0
C      JMAX = JJ
C      COPY SHIFT BACK INTO PTABEL:
C      NY7 = JMAX - 1
C      DO 1275 JJ = J, NY7
C      DO 1275 K = 1,7
C      1275 PTABEL(I2,JJ,K) = SHIFT(JJ+1,K)
C
C      RETURNING TO INCREMENTAL PART WITHOUT INCREASE IN J:
C      GO TO 1260
C
C      REMOVING LONGEST LIVING PUFF FROM SOURCE(I2):
C      1265 PTABEL(I2,J,1) = 0
C      CONTINUING WITH NEXT SOURCE
C      GO TO 1300
C
C      REPLACING NEW PUFF POSITION IN PUFF TABLE
C      1290 PTABEL(I2,J,3) = PTBL3
C      PTABEL(I2,J,4) = PTBL4
C
C      CALCULATING GRID CONCENTRATION IN EACH BASIC ADVECTION STEP

```

```

PUF05870
PUF05880
PUF05890
PUF05900
PUF05910
PUF05920
PUF05940
PUF05950
PUF05980
PUF05990
PUF06000
PUF06010
PUF06020
PUF06030
PUF06040
PUF06050
PUF06060
PUF06070
PUF06080
PUF06090
PUF06100
PUF06110
PUF06120
PUF06130
PUF06140
PUF06150
PUF06160
PUF06170
PUF06180

PUF06200
PUF06210
PUF06220
PUF06230
PUF06240
PUF06250
PUF06260
PUF06270
PUF06280
PUF06290
PUF06300
PUF06330
PUF06340
PUF06350
PUF06380
PUF06390
PUF06420

```


RENAMING ESSENTIAL PARAMETERS:

DOSE IN CURRENT PUFF:

QI = PTABEL(I2,J,2)

SIGMA VALUES IN METERS:

SIGMXY = PTABEL(I2,J,6)

SIGMZ = PTABEL(I2,J,7)

CALCULATING MAXIMUM CONCENTRATION IN EACH PUFF CENTER

(PUFF-CHI-CENTER) IN DIMENSION: GRAM/M**3 :

CONSTANT : $(2 * \text{PHI})^{**}(3/2)$

CONST = 15.7496

PCHCEN = QI/(CONST*SIGMZ*SIGMXY**2)

SKIPPING SUMMATION SECTION IF CONCENTRATION IS TOO LOW

IF(PCHCEN.LT.CHEMIN) GO TO 1500

CALCULATING MAXIMUM RADIUS OF INTEREST FOR EACH PUFF:

MAXIMUM PUFF RADIUS IN METERS:

PFRMXY = SIGMXY * SQRT(-2.*ALOG(CHEMIN/PCHCEN))

PFRMZ = PFRMXY*SIGMZ/SIGMXY

X-DIRECTION:

PUFRGX = PFRMXY/DELX

Y-DIRECTION:

PUFRGY = PFRMXY/DELY

Z-DIRECTION:

PUFRGZ = PFRMZ/DELZ

DETERMINING START AND STOP GRID POINTS FOR ACCUMULATION OF
THE PUFFS IN QUESTION:

ISTRX = PTBL3 - PUFRGX + 1

ISTOPX = PTBL3 + PUFRGX

ISTRY = PTBL4 - PUFRGY + 1

ISTOPY = PTBL4 + PUFRGY

ISTRZ = PTBL5 - PUFRGZ + 1

ISTOPZ = PTBL5 + PUFRGZ

CONTROL FOR EXCEEDING GRID DIMENSIONS

IF(ISTRX.LT.XSB) ISTRX=XSB

IF(ISTOPX.GT.XLB) ISTOPX=XLB

IF(ISTRY.LT.YSB) ISTRY=YSB

IF(ISTOPY.GT.YLB) ISTOPY=YLB

IF(ISTRZ.LT.ZSB) ISTRZ=ZSB

IF(ISTOPZ.GT.ZLB) ISTOPZ=ZLB

PUF06430
PUF06440
PUF06450
PUF06460
PUF06470
PUF06480
PUF06490
PUF06510
PUF06520
PUF06530
PUF06540
PUF06550
PUF06560
PUF06570

PUF06590
PUF06600
PUF06610
PUF06620
PUF06630
PUF06640
PUF06650
PUF06660
PUF06670
PUF06680
PUF06690
PUF06700
PUF06710
PUF06720
PUF06730
PUF06740
PUF06750
PUF06760
PUF06770
PUF06780
PUF06790
PUF06800
PUF06810
PUF06820
PUF06830
PUF06840
PUF06850
PUF06860
PUF06870
PUF06880
PUF06890
PUF06900
PUF06910


```

C      UPPER LIMIT IN CASE OF SPECIFIED MIXING DEPTH:ZM
C      IF(.NOT.NOMXDP .AND. ISTOPZ.GT. ZMG ) ISTOPZ = ZMG
C      IF(ISTRIZ .GT. ISTOPZ) GO TO 1500
C      CALCULATE CONTRIBUTIONS TO SURROUNDING GRIDPOINTS
C      PRELIMINAR CALCULATIONS:
C      SIGMAS IN GRIDUNITS:
C      SIGGX = SIGMX/DELX
C      SIGGY = SIGMY/DELY
C      SIGGZ = SIGMZ /DELZ
C      CALCULATING DENOMINATOR UNDER EXP-SIGN:
C      SIGGX2 = (SIGGX**2)*(-2)
C      SIGGY2 = (SIGGY**2)*(-2)
C      SIGGZ2 = (SIGGZ**2)*(-2)
C      LOOPING THRU ALL GRIDPOINTS OF INTEREST:
C      DO 1500 KG = ISTRIZ, ISTOPZ
C      ZG2NEG = (KG-PTBL5)**2
C      PCHI1 = PCHCEN * EXP(ZG2NEG/SIGGZ2)
C      IF(GRRFLX) PCHI1 = PCHI1 + PCHCEN*REFLEC*EXP((KG+PTBL5)**2/SIGGZ2)
C      IF(NOMXDP) GO TO 1295
C      IF((PTBL5+PUFRGZ) .LT. ZMG) GO TO 1295
C      ZG2MX = (KG+PTBL5-2*ZMG)**2
C      PCHI1 = PCHI1 + PCHCEN*EXP(ZG2MX/SIGGZ2)
C      DO 1500 IG = ISTRIZ, ISTOPX
C      XG2 = (IG-PTBL3)**2
C      DO 1500 JG = ISTRIZ, ISTOPY
C      YG2 = (JG-PTBL4)**2
C      INDIVIDUAL PUFFS CONTRIBUTION : PCHI,GRAM/M**3
C      PCHI = PCHI1 * EXP(XG2/SIGGX2 + YG2/SIGGY2)
C      IF(PCHI.LT. CHEMIN) GO TO 1500
C      ACCUMULATING IN GRIDPOINTS:
C      CHI(IG+1,JG+1,KG+1) = CHI(IG+1,JG+1,KG+1) + PCHI
C      1500 CONTINUE
C      END OF CONCENTRATION CALCULATIONS
C      ADVANCE IN PUFF TABLE (J) DURING BASIC ADVECTION STEP
C      J = J + 1

```

PUF069940
 PUF069950
 PUF069960
 PUF069970
 PUF069990
 PUF070000
 PUF070100
 PUF070200
 PUF070300
 PUF070400
 PUF070500
 PUF070600
 PUF070700
 PUF070800
 PUF070900
 PUF071000
 PUF071100
 PUF071300
 PUF071400
 PUF071500
 PUF071600
 PUF071700
 PUF071800
 PUF071900
 PUF072000
 PUF072100
 PUF072200
 PUF072300
 PUF072400
 PUF072500
 PUF072600
 PUF072700
 PUF072800
 PUF072900
 PUF073000
 PUF073100
 PUF073200
 PUF073300
 PUF073400
 PUF073500
 PUF073600
 PUF073700
 PUF073800
 PUF074100
 PUF074400
 PUF074500
 PUF074600


```

C      MAX = JROWS - 1
C      OUTER LOOP THRU INTEGER Y-VALUES:
C      NY8=MAX+1      NY9=1,NY8
C      I2=NY9-1
C      MAXMI2 = MAX - I2
C      WRITE(6,1327) MAXMI2 , VERPLS
C
C      PLOTTING SOURCE POSITIONS
C      K1 = 0
C      DO 1330 J = 1,NRMULT
C      IF(MAX-I2 .NE. YSOURC(J) ) GO TO 1330
C      NUMBER OF SOURCES IN MAINLINE: K1
C      K1 = K1 + 1
C      CALL ISPACE(XSOURC(J),J)
C      SOURCE POSITIONS IN EACH MAINLINE: XINT(K1)
C      XINT(K1) = 10*XSOURC(J)
C      CONTINUE
C      1330
C
C      LOOPING 9 LINES DOWN TO NEXT MAINLINE:
C      DO 1345 NY10=1,10
C      IDECI=NY10-1
C      YLINE = 10*(MAX - I2) - IDECI + 10
C      IF(IDECI .GE. 1) WRITE(6,1326) VERFRM
C
C      SCANNING THRU WHOLE PUFF TABLE
C      DO 1340 II = 1,NRMULT
C      J = 0
C      1335 J = J + 1
C      IF(PTABEL(II,J,1) .EQ. 0) GO TO 1340
C      TRUNCATING Y-VALUE OF PUFF TO INTEGER:
C      YINT = PTABEL(II,J,4)*10 + 10.5
C
C      PRINTING "*" IN GRIDFRAME IF X-POSITION OF PUFF= NOT COINCIDE
C      WITH ONE OF THE SOURCE POSITIONS
C      IF( (YINT .NE. YLINE) .OR. (IDECI .NE. 0) ) GO TO 1338
C      COINCD = .FALSE.
C      INTEGER VALUE OF PUFFS X-POSITION: XINTPF
C      XINTPF = PTABEL(II,J,3) * 10 + .5
C      DO 1336 KK = 1,K1
C      IF(XINTPF .EQ. XINT(KK)) COINCD = .TRUE.
C      1336 IF(COINCD) GO TO 1335
C      STRING(XINTPF + 1) = SN1
C      GO TO 1335
C
C      1338 IF(YINT .NE. YLINE) GO TO 1335
C      PRINTING PUFF POSITIONS BETWEEN Y-GRID LINES:
C      XINTPF = PTABEL(II,J,3) * 10 + .5

```

PUF07960

PUF08000
PUF08010
PUF08020
PUF08030
PUF08040
PUF08050
PUF08060
PUF08070
PUF08080
PUF08090

PUF08110
PUF08120
PUF08130
PUF08140

PUF08160
PUF08170
PUF08180
PUF08190
PUF08200
PUF08210
PUF08220
PUF08230
PUF08240
PUF08250
PUF08260
PUF08270
PUF08280
PUF08290
PUF08300
PUF08310
PUF08320
PUF08330
PUF08340
PUF08350
PUF08360
PUF08370
PUF08380
PUF08400


```

C 1340 STRING(XINTPF + 1) = SN1
C 1341 GO TO 1335
C 1342 CONTINUE
C 1343 END OF PUFF TABLE LOOP.
C 1344
C 1345 WRITE(6,1325) STRING
C 1346 DO 1342 NST = 1,105
C 1347 STRING(NST) = BL
C 1348 CONTINUE
C 1349 RESET "SOURCE IN LINE COUNTER" XINT(KK)
C 1350 DO 1349 KK=1,10
C 1351 XINT(KK) = -1
C 1352 CONTINUE
C 1353 END OF PUFF POSITION PLOT.
C 1354 WRITE(6,1)
C 1355 WRITE(6,912) HORFRM
C 1400 CONTINUE
C 1401
C 1402 PLOTTING PUFFS IN "Y-Z FRAME";FOR COMMENTS REFER TO THE EQUI-
C 1403 VALENT "Y-X FRAME" PLOTTING DESCRIBED ABOVE.
C 1404
C 1405 WRITE(6,1)
C 1406 WRITE(6,1)
C 1407 WRITE(6,1)
C 1408 881 FORMAT(1H+,20X,15,10H SOURCE(S))
C 1409 WRITE(6,871) (12,12=ZSB,ZLB)
C 1410 WRITE(6,1)
C 1411 HRFRMZ : STRING CONTAINING HORIZONTAL GRID FRAME
C 1412 DO 1410 N = 1,105
C 1413 VRFRMZ(N) = BL
C 1414 VRPLSZ(N) = BL
C 1415 PARENT(N) = BL
C 1416 HRFRMZ(N) = BL
C 1417 NY11=MFZ*10
C 1418 DO 1418 IHFZ = MSZ,NY11,10
C 1419 NY12=IHFZ+4
C 1420 DO 1411 MN = IHFZ,NY12
C 1421 HRFRMZ(MN) = SN4
C 1422 HRFRMZ(IHFZ+5) = SN2
C 1423 NY13=IHFZ+6
C 1424 NY14=IHFZ+9
C 1425 DO 1416 MM=NY13,NY14
C 1426 HRFRMZ(MM) = SN4

```

PUF08430
 PUF08440
 PUF08450
 PUF08470
 PUF08480
 PUF08490
 PUF08500
 PUF08510
 PUF08520
 PUF08530
 PUF08540
 PUF08550
 PUF08570
 PUF08580
 PUF08590
 PUF08600
 PUF08610
 PUF08620
 PUF08630
 PUF08640
 PUF08650
 PUF08660
 PUF08670
 PUF08690
 PUF08700
 PUF08710
 PUF08720
 PUF08730
 PUF08740
 PUF08750
 PUF08760
 PUF08770
 PUF08780
 PUF08790
 PUF08800
 PUF08810
 PUF08820
 PUF08830
 PUF08840
 PUF08860
 PUF08870
 PUF08890


```

1418 CONTINUE
      WRITE(6,912) HRFRMZ
      PARENT(10*ZMG + 1) = SN6
      VRFRMZ(10*MFZ + 3) = SN5
      VRPLSZ(10*MFZ + 3) = SN3
      WRITE(6,1326) VRFRMZ
      WRITE(6,1326) VRFRMZ
      MAX = JROWS-1
      DO 1445 NY15=1,JROWS
        I2=NY15-1
        MAXMI2 = MAX - I2
        WRITE(6,1327) MAXMI2,VRPLSZ
        K1=0
        DO 1430 J=1,NRMULT
          IF (MAX-I2 .NE. YSOURC(J)) GO TO 1430
          K1 = K1+1
          CONTINUE
          C
          1430 WRITING NUMBER OF SOURCES IN EACH Y-GRIDLINE: VN SOURCE(S)
          IF(K1.GT.0) WRITE(6,881) K1
          DO 1445 NY16=1,10
            IDECI=NY16-1
            YLINE = 10*(MAX-I2) - IDECI +10
            IF(IDECI.GE.1) WRITE(6,1326) VRFRMZ
            C
            ILLUSTRATING MIXING DEPTH IN Y-Z FRAME:
            IF(ZMG.GT.0) WRITE(6,1328) PARENT
            DO 1440 II = 1,NRMULT
              J=0
              1435 J = J + 1
              IF(PTABEL(II,J,1) .EQ. 0) GO TO 1440
              YINT = PTABEL(II,J,4) *10 + 10.5
              IF(YINT .NE. YLINE) GO TO 1435
              C
              ZINTPF = PTABEL(II,J,5)* 10 + .5
              STRING(ZINTPF + 1) = SN1
              GO TO 1435
              C
              1440 CONTINUE
              C
              1440 CONTINUE
              WRITE(6,1325) STRING
              DO 1442 NST = 1,105
                1442 STRING(NST) = BL
                C
                1445 CONTINUE
                C
                WRITE(6,1)
                WRITE(6,912) HRFRMZ
                C
                C SECTION FOR OUTPRINTING GRID CONCENTRATIONS

```

PUF 08900
 PUF 08910
 PUF 08920
 PUF 08930
 PUF 08940
 PUF 08950
 PUF 08960
 PUF 08970
 PUF 08980
 PUF 08990
 PUF 09000
 PUF 09010
 PUF 09020
 PUF 09030
 PUF 09040
 PUF 09050
 PUF 09060

PUF 09080
 PUF 09090
 PUF 09110
 PUF 09120
 PUF 09130
 PUF 09140
 PUF 09150
 PUF 09160
 PUF 09170
 PUF 09180
 PUF 09190
 PUF 09200
 PUF 09210
 PUF 09220
 PUF 09230
 PUF 09240
 PUF 09250
 PUF 09260
 PUF 09270
 PUF 09280
 PUF 09290
 PUF 09300
 PUF 09310
 PUF 09320
 PUF 09330
 PUF 09350


```

C          SKIPPING CONCENTRATION PRINTING IF SPECIFIED IN PRIMDA.
C          IF(ABC(9).EQ. NO ) GO TO 1600
C
C 1510  FORMAT(1H0,49X,37H PRINT OF CURRENT GRID CONCENTRATIONS,/50X
C 116,29H SEC. AFTER START OF RELEASE.)
C 1520  FORMAT(1H0,49X,32H GRIDCONCENTRATION IN THE PLANE:,/51X,3HZ =F6.2
C 11,25H METER ABOVE THE SURFACE.)
C 1525  FORMAT(11,8X,10E10.2)
C          WRITE(6,1301)
C          WRITE(6,1510) ITOTIM
C          WRITE(6,1)
C          WRITE(6,1)
C          LOOP THRU ALL Z LEVELS
C
C          DO 1550  KC=1,KPLANS
C          DEMKMI = DELZ*(KC-1)
C          WRITE(6,1520) DEMKMI
C          WRITE(6,1)
C          WRITE(6,870) (IC,IC = XSB,XLB)
C          PRINTING EACH LINE IN CONCENTRATION TABLE:
C          DO 1560  JC = 1,JROWS
C          JJC = JRCWS - JC
C          JCL = JJC + 1
C          WRITE(6,1525) JJC, (CHI(IC,JCL,KC) , IC = MSX,MFX)
C          DO 1551  IC=MSX,MFX
C          CPLOT(IC,JCL)=CHI(IC,JCL,KC)
C          1551  CPLOT(IC,JCL)=CHI(IC,JCL,KC)
C          1552  FORMAT(5X,10E10.2)
C          1560  CONTINUE
C
C          KC IS THE NO. OF LEVELS PRINTED...HERE CONTROLS WHICH
C          LEVELS ARE CONTOURED.
C          IF (KC.EQ.1) CALL DRAW(CPLOT,10,17)
C
C 1550  CONTINUE
C          WRITE(6,1)
C          WRITE(6,1)
C          GO TO 1600
C
C 1590  FORMAT(95H PUFF POSITION PLOT AND GRID CONCENTRATION PRINTING AR
C 1E SUPPRESSED BECAUSE "ICOLS" EXCEED 10.)
C 1595  WRITE(6,1590)
C
C 1600  CONTINUE
C          END OF GRID CONCENTRATION PRINTING SECTION
C

```

```

PUF09360
PUF09380
PUF09390
PUF09410
PUF09420
PUF09430
PUF09440
PUF09450
PUF09460
PUF09470
PUF09480
PUF09490
PUF09500
PUF09510
PUF09520
PUF09530
PUF09540
PUF09550
PUF09560
PUF09570
PUF09580
PUF09590
PUF09600
PUF09610
PUF09620
PUF09630
PUF09640
PUF09650
PUF09670
PUF09680

PUF09690
PUF09710
PUF09720
PUF09730
PUF09750
PUF09760
PUF09770
PUF09780
PUF09790
PUF09800
PUF09830
PUF09840
PUF09870

```



```

8930 WRITE(6,1140)
      GO TO 9999
8940 NRM1 = NRSTAB - 1
      WRITE(6,1030) NRM1
      GO TO 9999
8950 WRITE(6,1025) NRSTAB
      GO TO 9999
8970 WRITE(6,1015) WINDAV,NTADV
      GO TO 9999
8980 WRITE(6,1010) TAU,NTADV
      GO TO 9999
8990 WRITE(6,1005)
      GO TO 9999
9000 WRITE(6,1000) I
C
9999 CONTINUE
      CALL EFRAME
      STOP
      END

```

PUF10410
 PUF10420
 PUF10430
 PUF10440
 PUF10450
 PUF10460
 PUF10470
 PUF10480
 PUF10490
 PUF10500
 PUF10510
 PUF10520
 PUF10530
 PUF10540
 PUF10550
 PUF1A160

```

SUBROUTINE SIGRIS(HGN,SIGXY,SIGZ)

```

PUF10570
 PUF10580
 PUF10590
 PUF10600
 PUF10610
 PUF10640
 PUF10650
 PUF10660
 PUF10690
 PUF10700
 PUF10710
 PUF10720
 PUF10730
 PUF10740
 PUF10750
 PUF10760
 PUF10780
 PUF10790
 PUF10800

```

THE SUBROUTINE "SIGRIS" (SIGMA-RISE) CALCULATES THE INCREMENT
IN SIGMA-XY AND SIGMA-Z DURING EACH BASIC ADVECTION STEP.
FURTHER, THE SUBROUTINE ESTIMATES PLUMERISE ASSOCIATED WITH
BOUYANCY IN THE EFFLUXES.

```

```

FOR Z-COORDINATES OF PUFFS: HEIGHT , GRID UNITS(N) : HGN

```

```

COMMON HEATFX(25),I2,DMS,POINT,INTENS(14),STABPA,FBUFLX

```

```

1  UNN,CONST1,DELZ

```

```

      REAL POINT

```

```

      REAL INTENS

```

```

      CALCULATING GROWTH RATES FOR SIGMAS; DSIGDS

```

```

      DEFINING EXPERIMENTAL FITTING CONSTANT: FITCST

```

```

      FITCST = 2.0

```

```

      DSIGDS = .22 * INTENS(POINT)

```

```

      DSIGDS = DSIGDS * FITCST

```

```

      SIGXY = SIGXY + DSIGDS * DMS

```

```

      SIGZ = SIGZ + DSIGDS * DMS

```

```

      CALCULATING PLUME-RISE INCREMENT:

```

PUF10810
 PUF10820
 PUF10830
 PUF10850
 PUF10860
 PUF10870
 PUF10880
 PUF10890
 PUF10900
 PUF10910


```

      RETURN
1  IF(IITENFT.NE.1) GO TO 2
   WRITE(6,20) INR
   RETURN
2  IF(IITENFT.NE.2) GO TO 3
   WRITE(6,30) INR
   RETURN
3  IF(IITENFT.NE.3) GO TO 4
   WRITE(6,40) INR
   RETURN
4  IF(IITENFT.NE.4) GO TO 5
   WRITE(6,50) INR
   RETURN
5  IF(IITENFT.NE.5) GO TO 6
   WRITE(6,60) INR
   RETURN
6  IF(IITENFT.NE.6) GO TO 7
   WRITE(6,70) INR
   RETURN
7  IF(IITENFT.NE.7) GO TO 8
   WRITE(6,80) INR
   RETURN
8  IF(IITENFT.NE.8) GO TO 9
   WRITE(6,90) INR
   RETURN
9  IF(IITENFT.NE.9) GO TO 1000
   WRITE(6,100) INR
1000 RETURN
      END

```

C C C C C C C C C C

SUBROUTINE DRAW (A,M,N)

THIS SUBROUTINE CONVERTS THE GRID CONCENTRATIONS TO LOG VALUES
THEN SMOOTHES AND CONTOURES THE PUFF ARRAY...

DIMENSION A(M,N)

A IS THE ARRAY TO BE SMOOTHED AND CONTOURED
M,N IS THE DIMENSION OF ARRAY A

```

DO 1553 JC=1,N
JJC=N-JC
JCI=JJC+1
DO 1554 IC=1,M
IF(A(IC,JCI):LT.1E-12) A(IC,JCI)=0.0
A(IC,JCI)=A(IC,JCI)*1.E13

```

PUF11740

PUF11430
PUF11440
PUF11450
PUF11460
PUF11470
PUF11480
PUF11490
PUF11500
PUF11510
PUF11520
PUF11530
PUF11540
PUF11550
PUF11560
PUF11570
PUF11580
PUF11590
PUF11600
PUF11610
PUF11620
PUF11630
PUF11640
PUF11650
PUF11660
PUF11670
PUF11680
PUF11690
PUF11700
PUF11710
PUF11720


```

IF(A(IC,JCL).EQ.0.0) GO TO 1554
A(IC,JCL)=ALOG10(A(IC,JCL))
CONTINUE
1554 WRITE(6,1555) (A(IC,JCL),IC=1,M)
1553 FORMAT(5X,10E10.2)
1555 SMOOTH ARRAY
MM1=M-1
NMI=N-1
DO 200 J=1,N
TEMP=A(I,J)
DO 100 I=2,MM1
TEMP1=A(I,J)
A(I,J)=.20*(TEMP+3.*TEMP1+A(I+1,J))
TEMP=TEMP1
CONTINUE
100 CONTINUE
DO 400 I=1,M
TEMP=A(I,1)
DO 300 J=2,NMI
TEMP1=A(I,J)
A(I,J)=.20*(TEMP+3.*TEMP1+A(I,J+1))
TEMP=TEMP1
CONTINUE
300 CONTINUE
400 CONTINUE
DO 1559 J=1,17
WRITE(6,1555) (A(I,J),I=1,10)
CALL SET (.1,.31,.2,.58,0.1,0.1,0.1,0.1,0.1,0.1)
CALL CONREC(A,10,10,17,0.0,0.1,0.1,-1,-1,0)
CALL TICK4(5,8,5,8)
CALL PERIM(9,0,16,0)
CALL FRAME
RETURN
END

```

PUF11750

PUF11760
PUF11770
PUF11780
PUF11790
PUF11800
PUF11810
PUF11820
PUF11830
PUF11840
PUF11850
PUF11860

SUBROUTINE RSPACE(ITENFT,RNR)
THIS SUBROUTINE HAS THE SAME PURPOSE FOR REAL FIGURES, AS
ISPACE HAS FOR INTEGER FIGURES.

RNR : REAL NUMBER TO BE PRINTED.

```

10 FORMAT(1H+,19X,F6.1)
20 FORMAT(1H+,29X,F6.1)
30 FORMAT(1H+,39X,F6.1)
40 FORMAT(1H+,49X,F6.1)

```

CCCC CCCCCC

PUF11870
 PUF11880
 PUF11890
 PUF11900
 PUF11910
 PUF11920
 PUF11930
 PUF11940
 PUF11950
 PUF11960
 PUF11970
 PUF11980
 PUF11990
 PUF12000
 PUF12010
 PUF12020
 PUF12030
 PUF12040
 PUF12050
 PUF12060
 PUF12070
 PUF12080
 PUF12090
 PUF12100
 PUF12110
 PUF12120
 PUF12130
 PUF12140
 PUF12150
 PUF12160
 PUF12170
 PUF12180
 PUF12190
 PUF12200
 PUF12210
 PUF12220
 PUF12230
 PUF12240
 PUF12250

50 FORMAT(1H+,59X,F6.1)
 60 FORMAT(1H+,69X,F6.1)
 70 FORMAT(1H+,79X,F6.1)
 80 FORMAT(1H+,89X,F6.1)
 90 FORMAT(1H+,99X,F6.1)
 100 FORMAT(1H+,109X,F6.1)

C C

IF (ITENFT.NE.0) GO TO 1
 WRITE(6,10) RNR
 RETURN
 1 IF (ITENFT.NE.1) GO TO 2
 WRITE(6,20) RNR
 RETURN
 2 IF (ITENFT.NE.2) GO TO 3
 WRITE(6,30) RNR
 RETURN
 3 IF (ITENFT.NE.3) GO TO 4
 WRITE(6,40) RNR
 RETURN
 4 IF (ITENFT.NE.4) GO TO 5
 WRITE(6,50) RNR
 RETURN
 5 IF (ITENFT.NE.5) GO TO 6
 WRITE(6,60) RNR
 RETURN
 6 IF (ITENFT.NE.6) GO TO 7
 WRITE(6,70) RNR
 RETURN
 7 IF (ITENFT.NE.7) GO TO 8
 WRITE(6,80) RNR
 RETURN
 8 IF (ITENFT.NE.8) GO TO 9
 WRITE(6,90) RNR
 RETURN
 9 IF (ITENFT.NE.9) GO TO 1000
 WRITE(6,10) RNR
 RETURN
 1000 RETURN

//GO.FT01F001 DD *
 12 3600 0 10 17 4 1
 3600 40 90
 PRIMDATA SEPT 29 81
 217.50 435.00 40.00 1.000E-13 1.0000
 YES
 YES
 YES
 YES


```

INST
//GO.FT02E001 DD UNIT=SYS DA, DISP=(OLD,DELETE), DSN=&FT02
//GO.FT03F001 DD *
STABILITY-DATA, SEPT 29 81
1.0000
80.00
//GO.FT04F001 DD *
INDIVIDUAL SOURCE DATA
#01# 1 2 0 0 3600 6.04 15.07 4.0
//GO.SYSIN DD *
INTENSITY-DATA, SEPT 29 81
#5#
.2500.1000.0500.0100.0300

```


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Silver Springs, MD 20910
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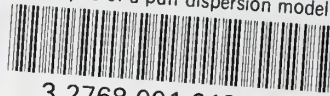
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